

Mind the Gap

TMT 2018, November 2018, Cologne, Germany

tmt30

SPECIMEN

DISCLAIMER



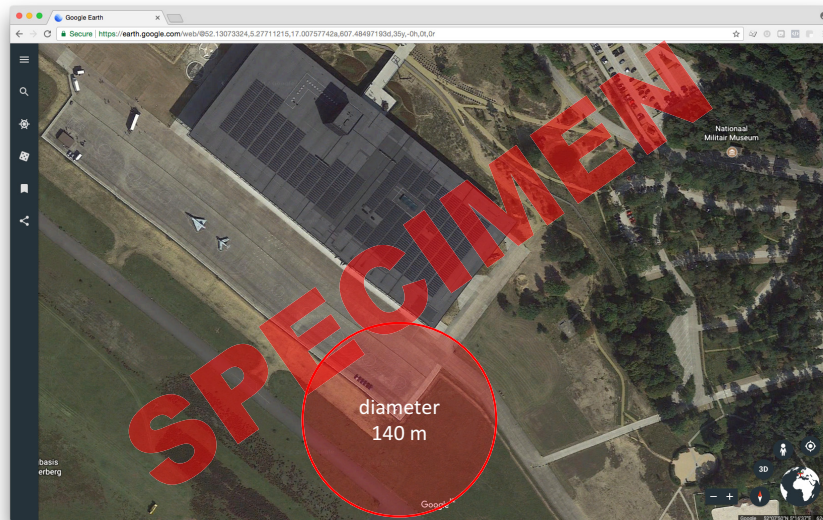
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These views, thoughts and opinions are subject to change, revision, and rethinking at any time.

Former Air Force Base "Soesterberg" NL

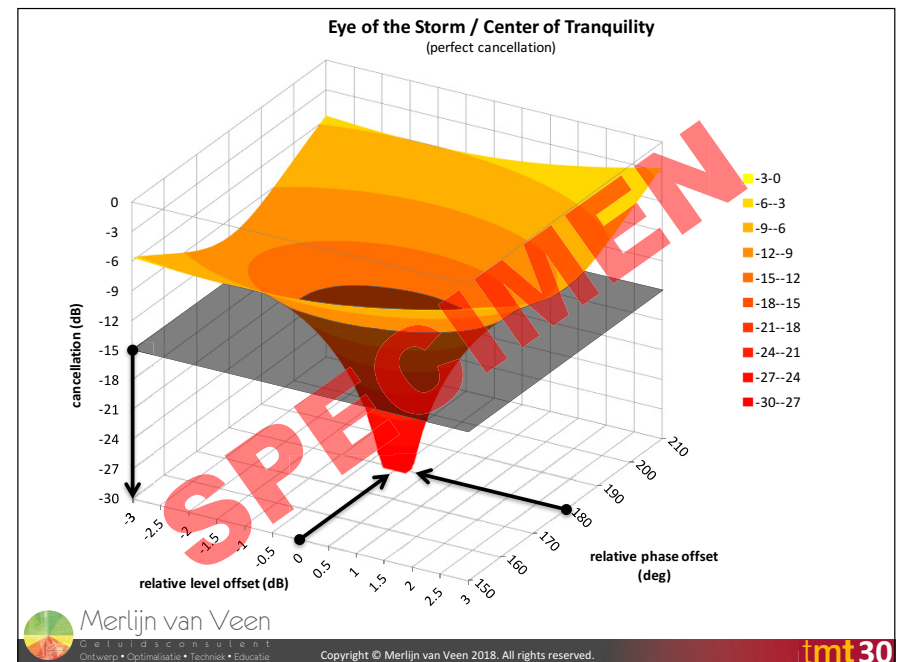
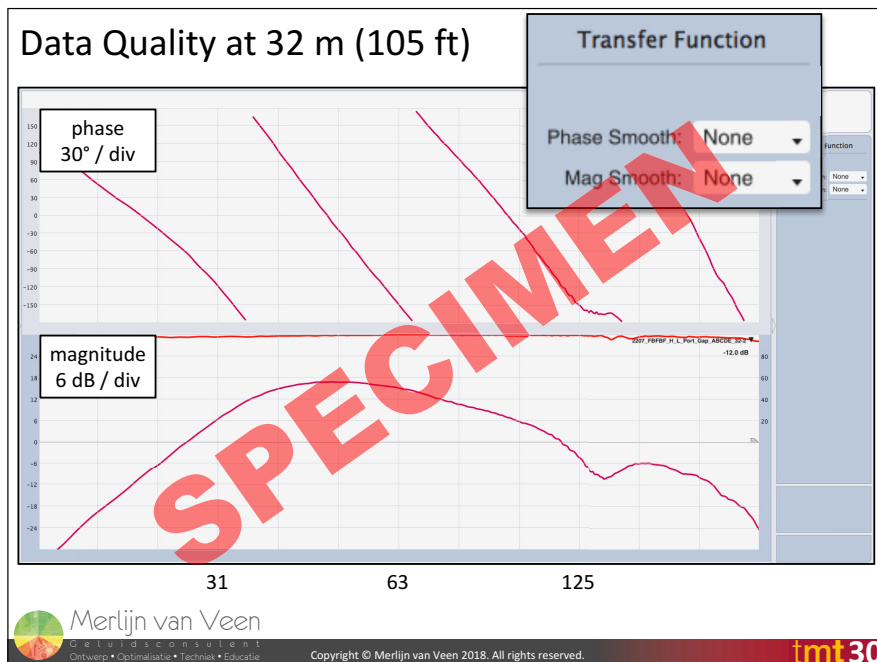
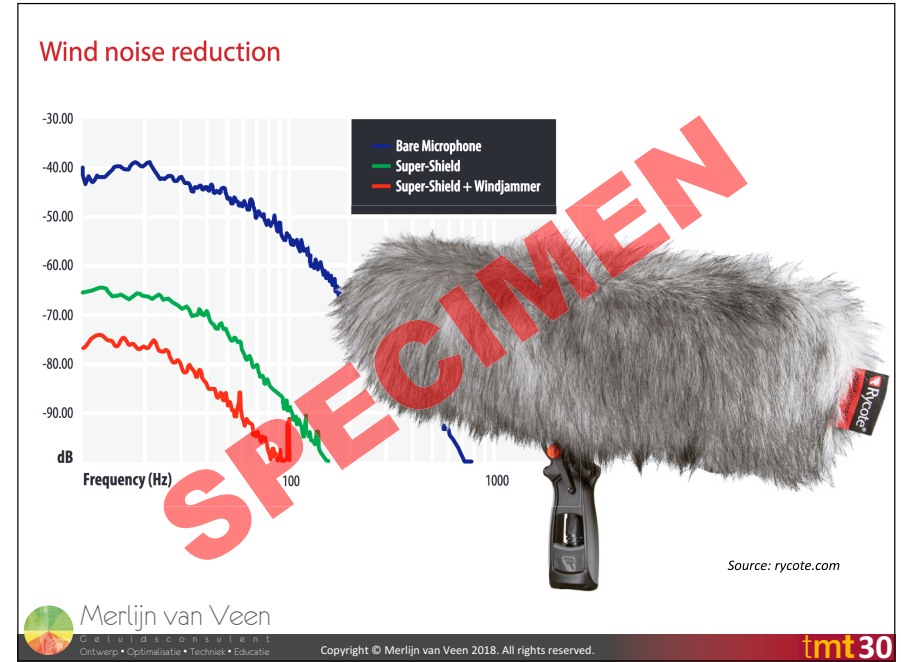
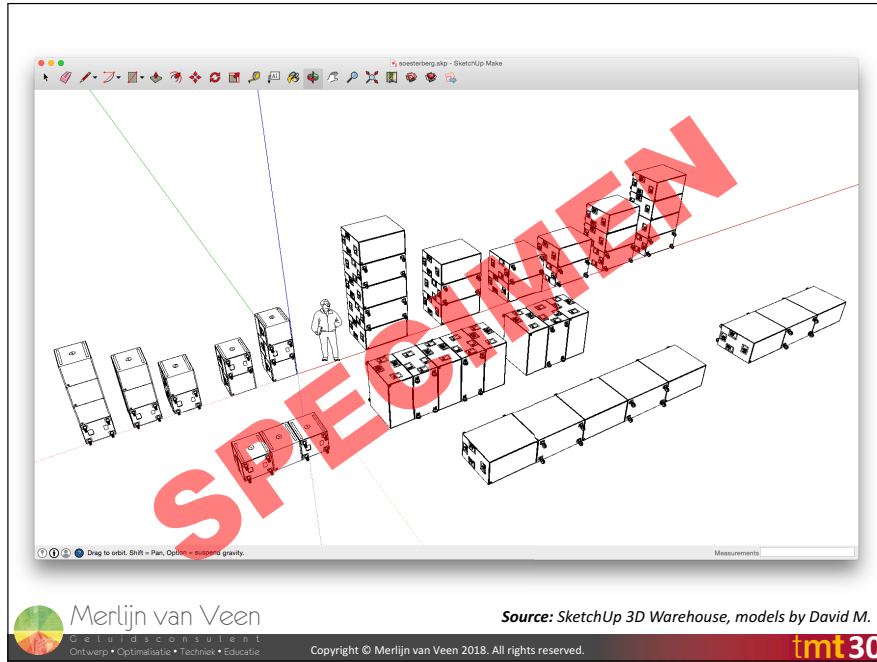
(Summer 2017)

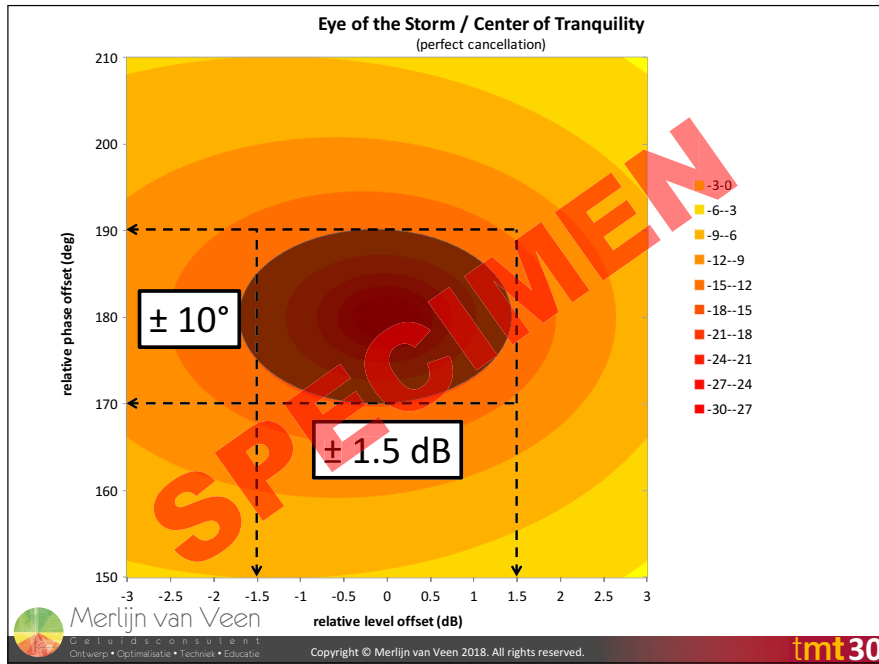


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(Summer 2017)







Gradient Array

by Harry Olson
1972

Harry F. Olson
P.O. Laboratories, Princeton, N. J.

Gradient Loudspeakers*

1972. Directional loudspeakers depend upon the difference in phase, between two drivers. The directivity of the conventional wave-type loudspeakers depends mainly on the interference of the sound emanating from the elements of the radiating surface. To obtain any measure of directivity from the wave-type loudspeaker, the radiating surface must be comparable to the wavelength. Therefore, the directivity of the wave-type loudspeakers becomes limited to the low audio frequency range. In various gradient-type loudspeakers an array, compared to the wave-type loudspeaker, provides the features of relatively small size and uniform directivity with respect to frequency.

INTRODUCTION: Directional loudspeakers may be divided into two classes, first, wave-type loudspeakers which depend for directivity in some manner upon wave interference of the sound emanating from the elements of the radiating surface and second, gradient-type loudspeakers which depend for directivity upon the difference in phase in the general sound pressure or power of the difference in phase at two points in space. In the first class of loudspeakers, which is the common one, in which the directivity depends in some way upon wave interference to obtain any measure of directivity the dimensions of the radiator must be comparable to the wavelength of the sound wave. The radiator in this class of loudspeaker is the surface of the cone of a direct-radiator loudspeaker, the mouth of the horn of a horn loudspeaker, the array of direct-radiator loudspeakers or the array of horn loudspeakers. The dimensions of gradient loudspeakers as compared to the wavelength, the above indicates the difficulty of obtaining directivity in the wave-type systems in low-frequency range without use of very large systems. Directional loudspeakers are very useful in sound reinforcement systems for the reduction of the effective radiative area and feedback. This is particularly true in the case of speech reinforcement where the level of the original sound is relatively low. Gradient loudspeakers are especially suited for speech reproduction since the extreme low-frequency range is somewhat limited.

The purpose of this paper is to describe gradient loudspeaker systems.

THEORETICAL CONSIDERATIONS

To provide the fundamental principles of gradient loudspeakers, a brief theoretical consideration of the

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Presented November 12, 1972, at the 48th Convention of the Audio Engineering Society, New York.

*The term gradient loudspeaker is used to designate a loudspeaker consisting of two drivers separated in space and operated with a difference in phase or reverse of the difference in phase between the radiators. The wave differential loudspeaker class of gradient loudspeakers could also be used to produce gradient directivity in speakers for the reproduction of audio reproduction systems. However, this includes the use of the term gradient loudspeakers.

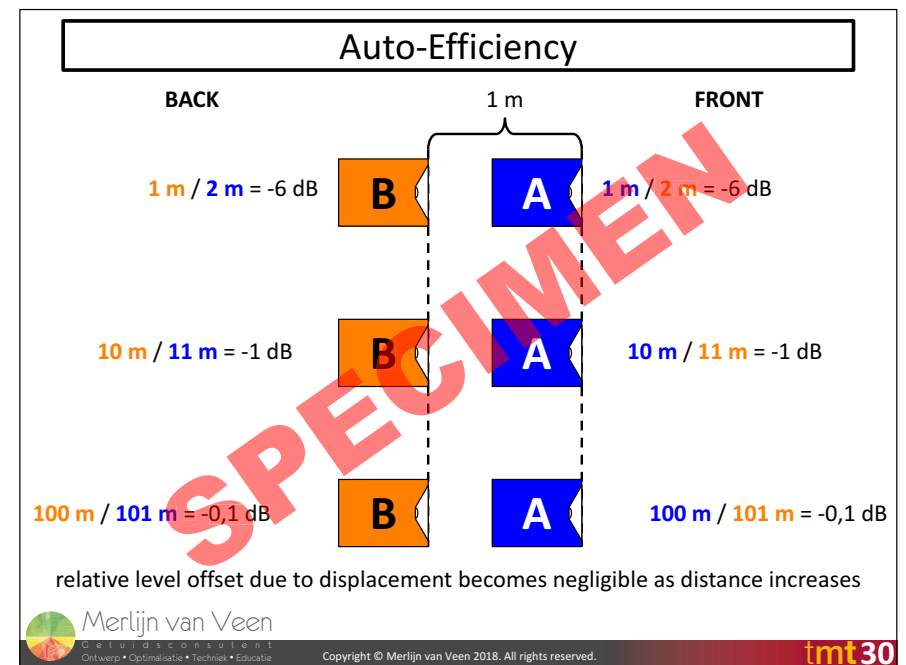
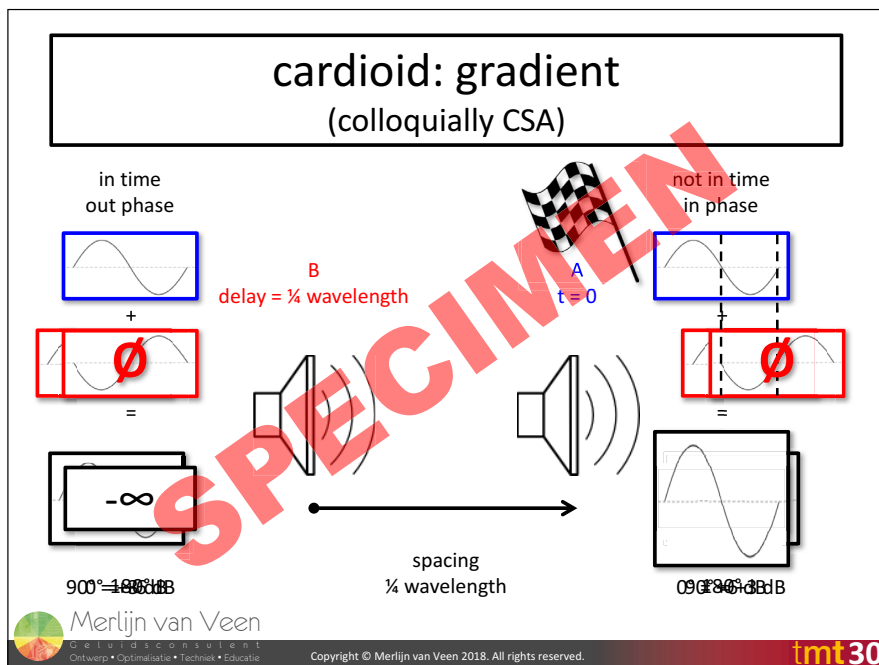
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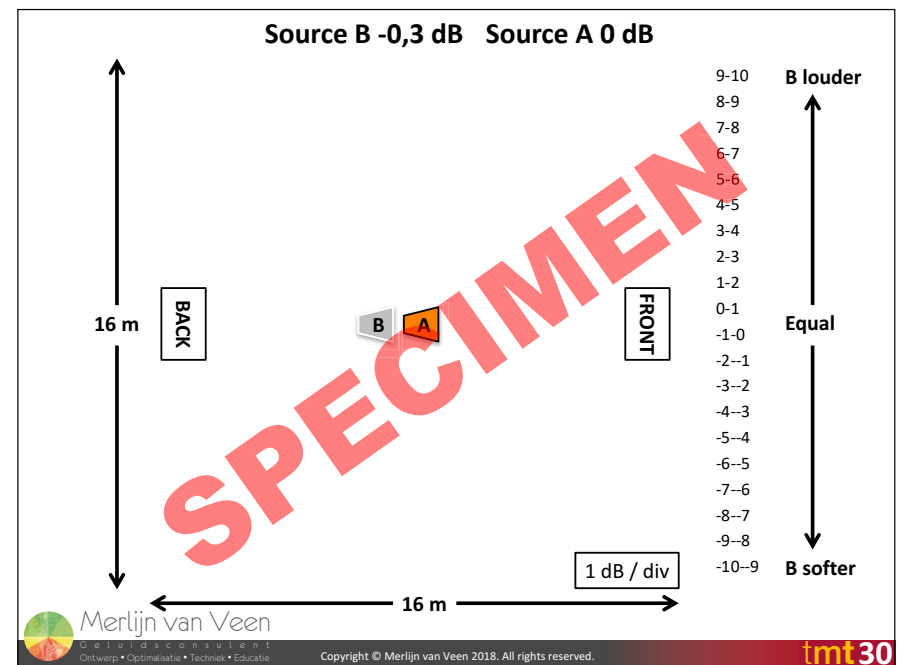
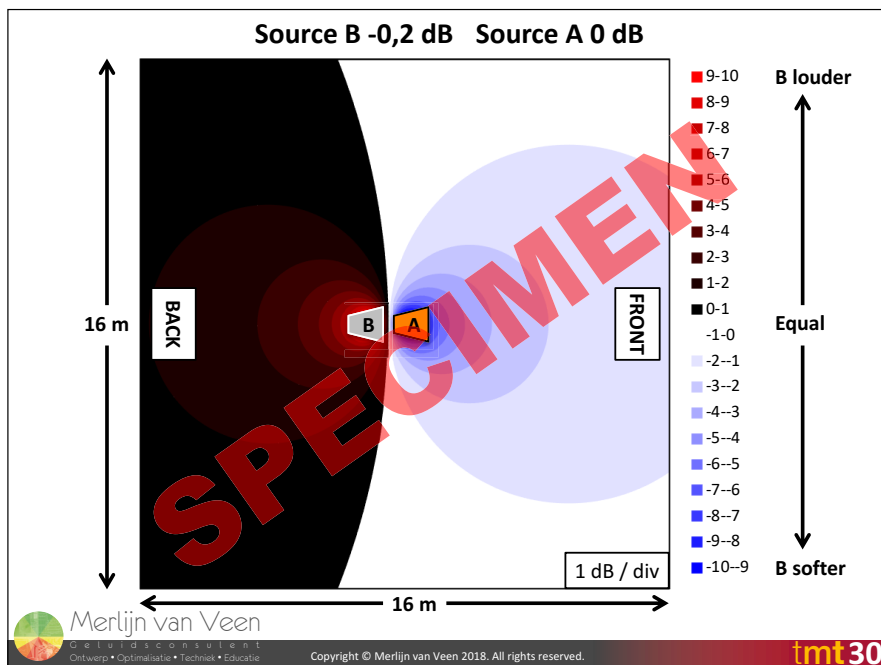
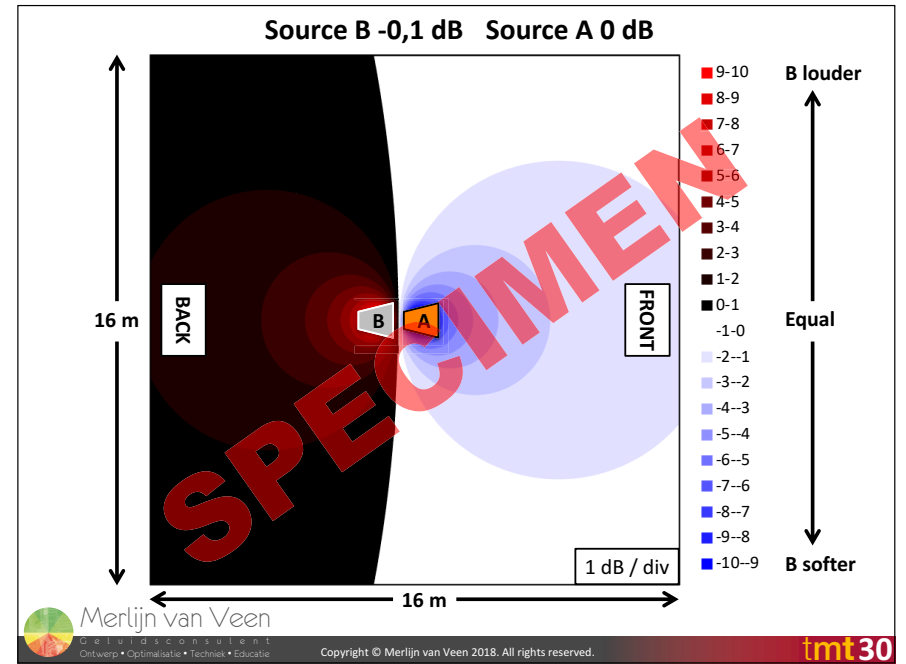
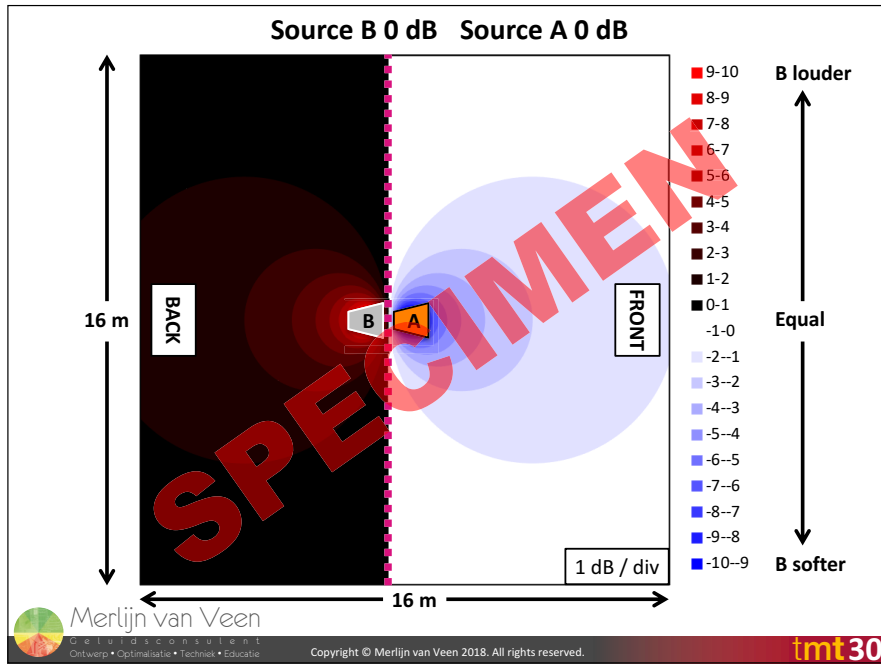
inverted stack

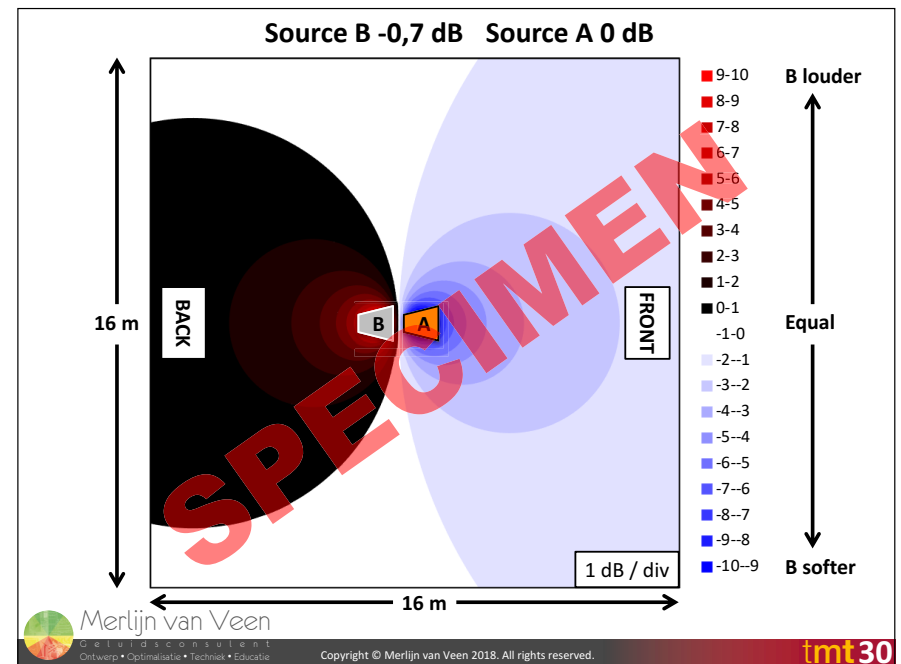
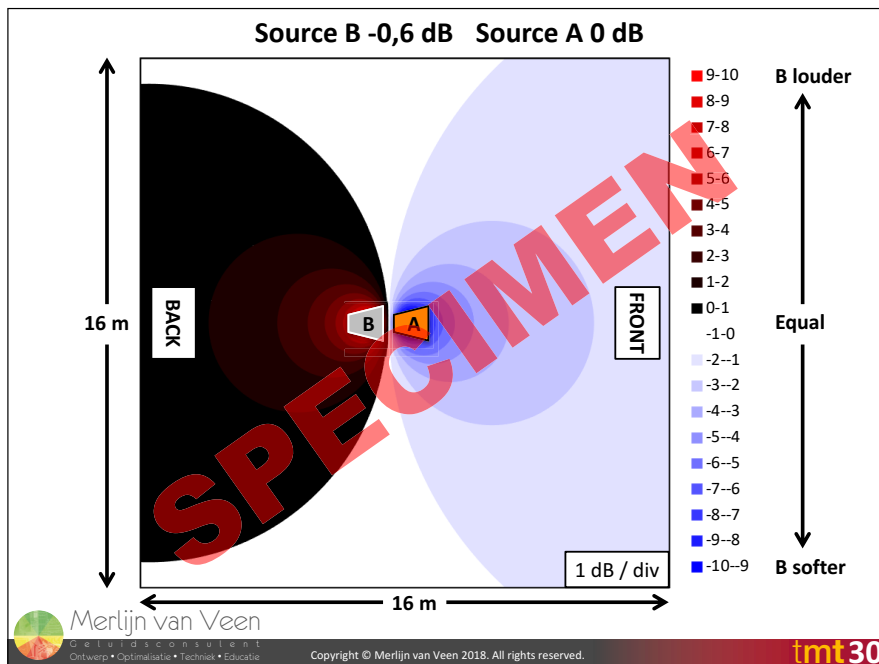
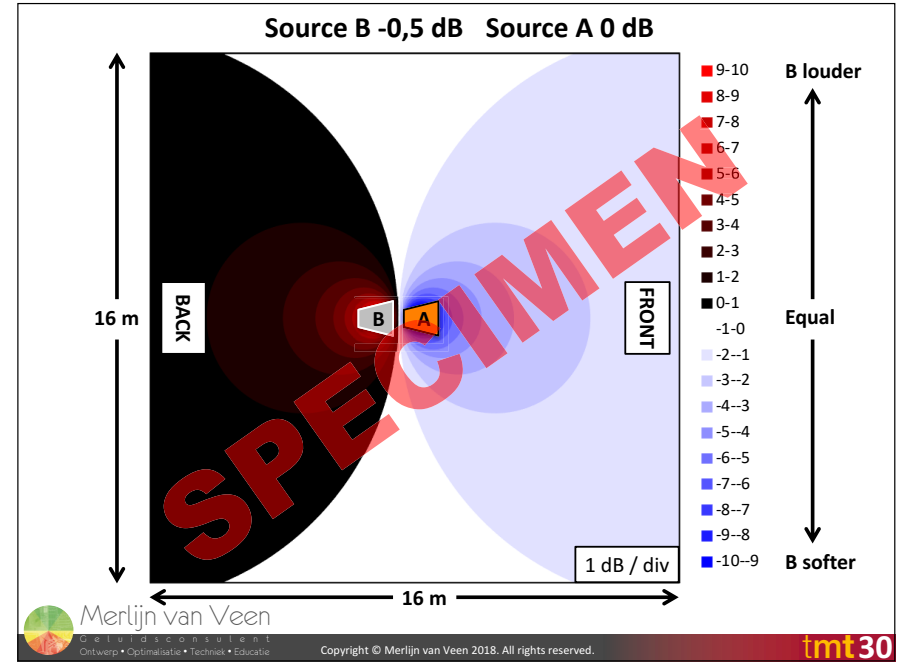
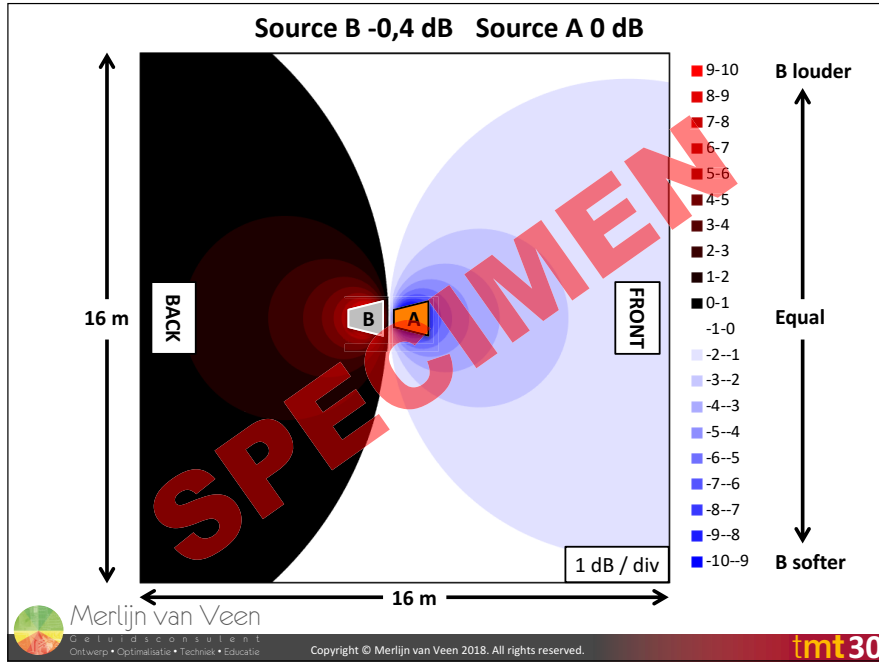
Source: SketchUp 3D Warehouse

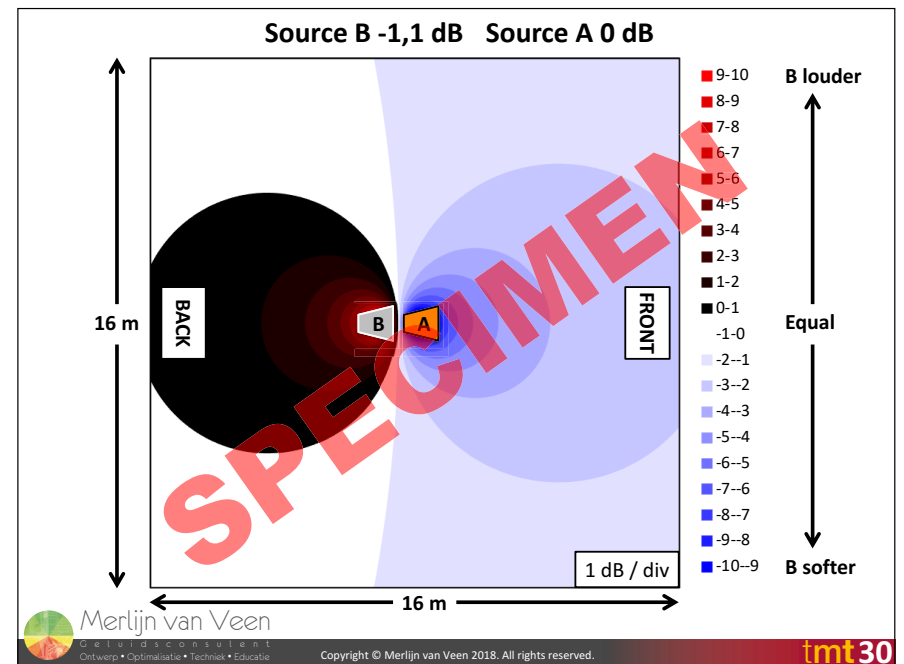
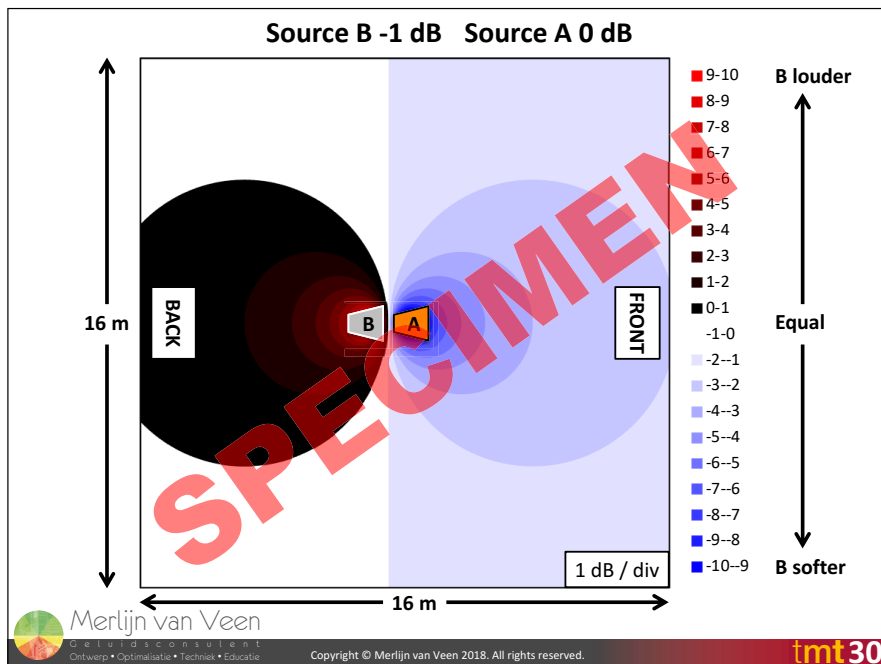
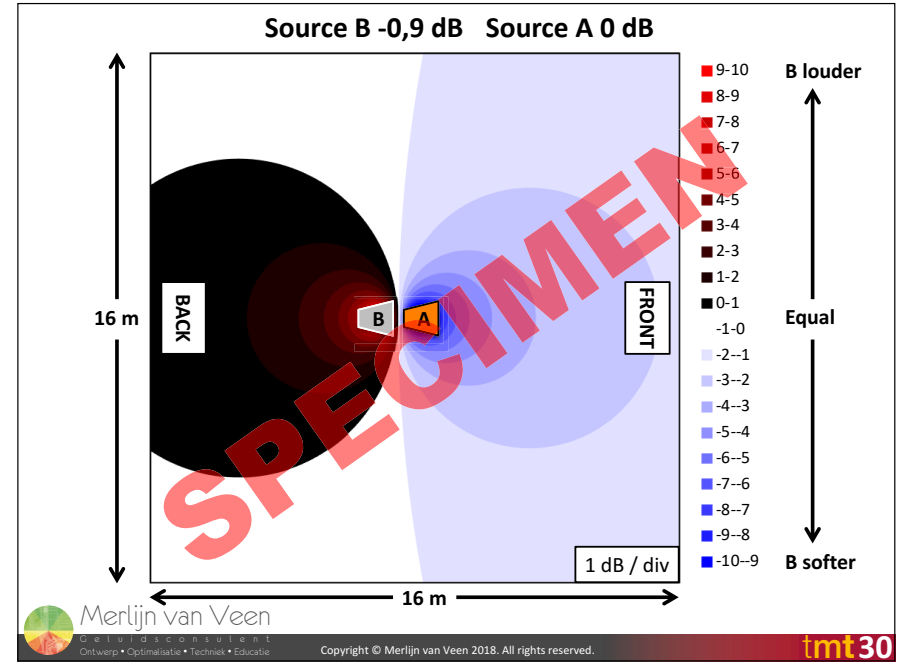
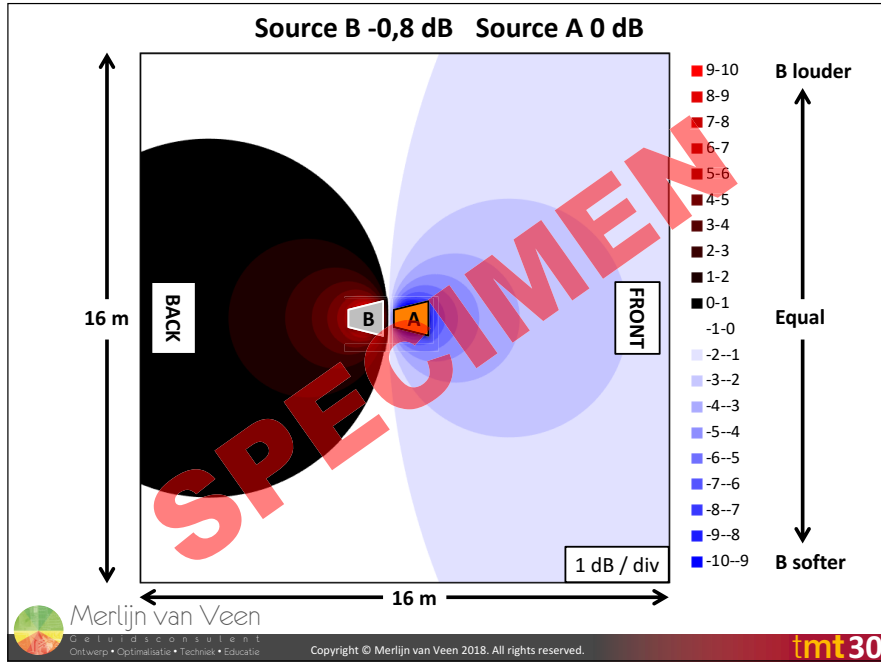
Merlijn van Veen
G e l u i d s c o n s u l t
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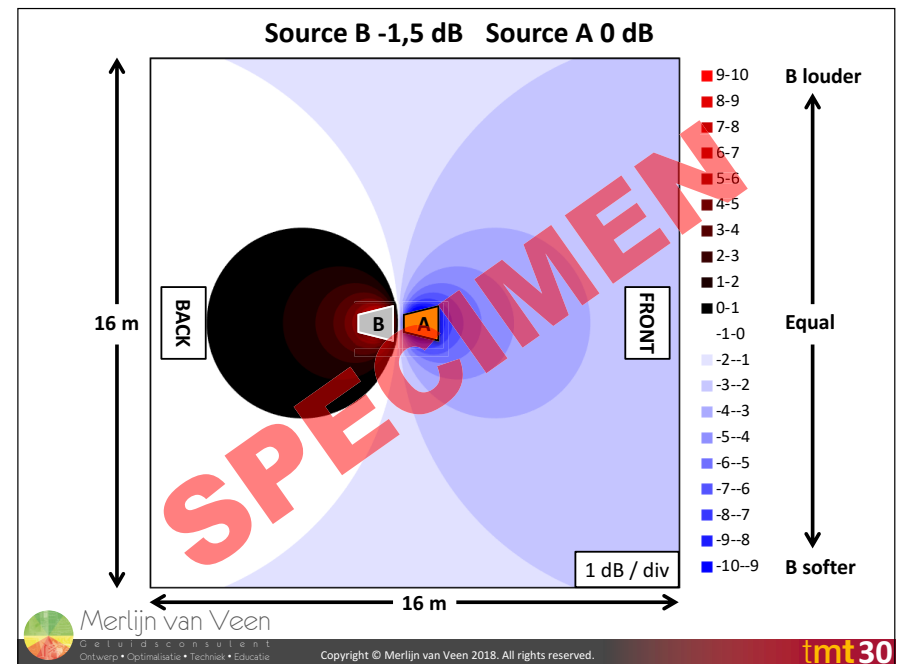
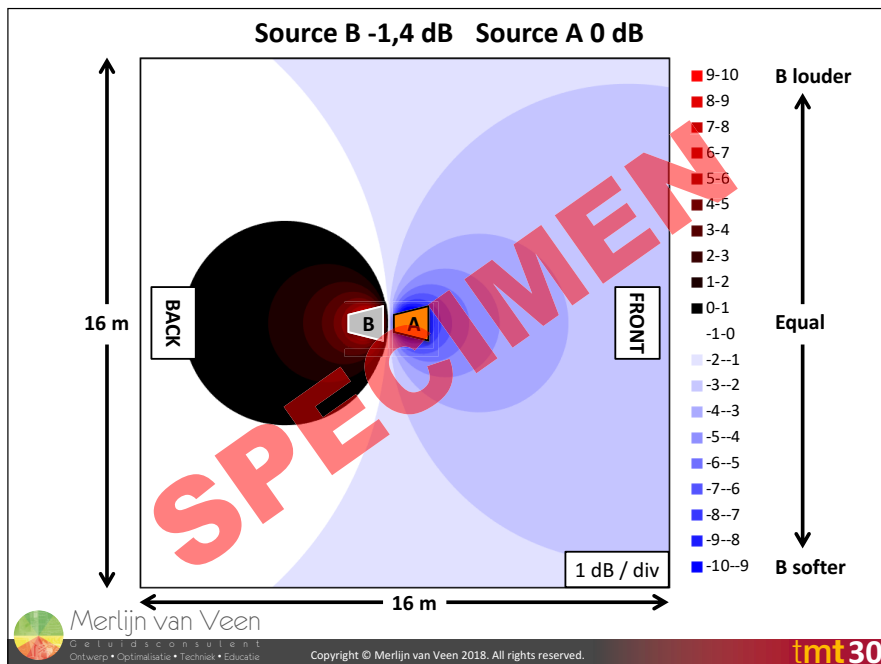
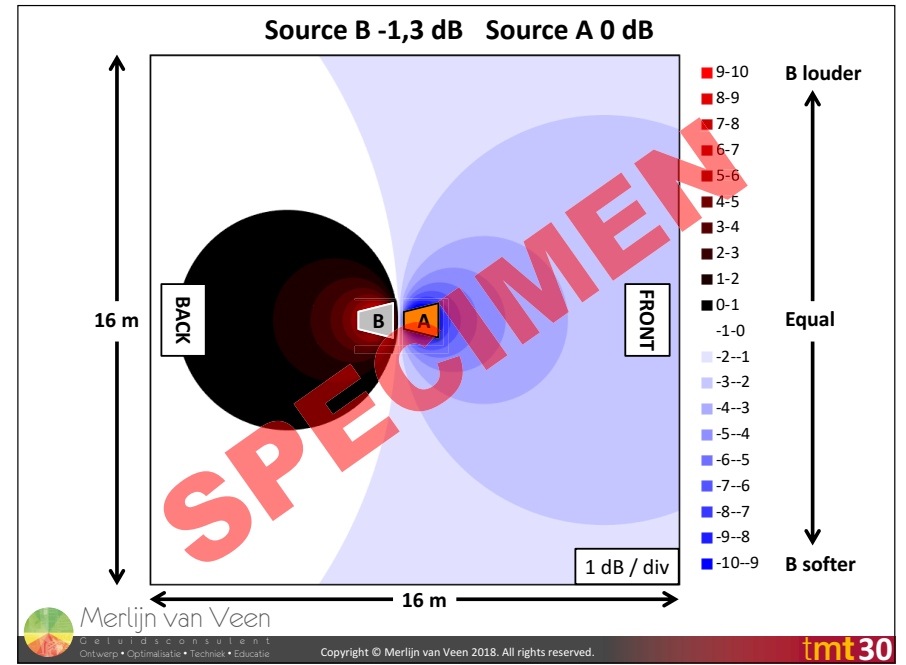
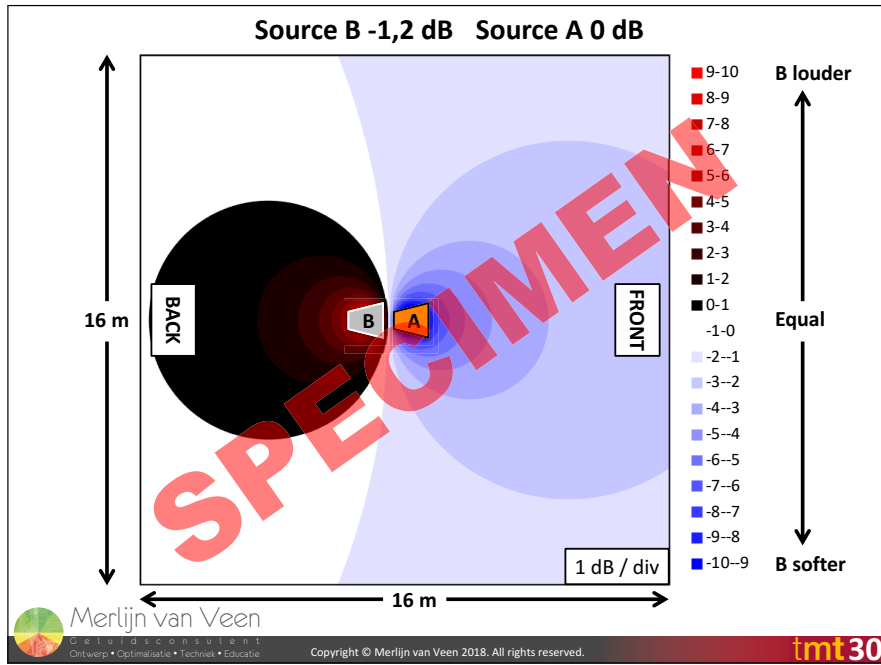
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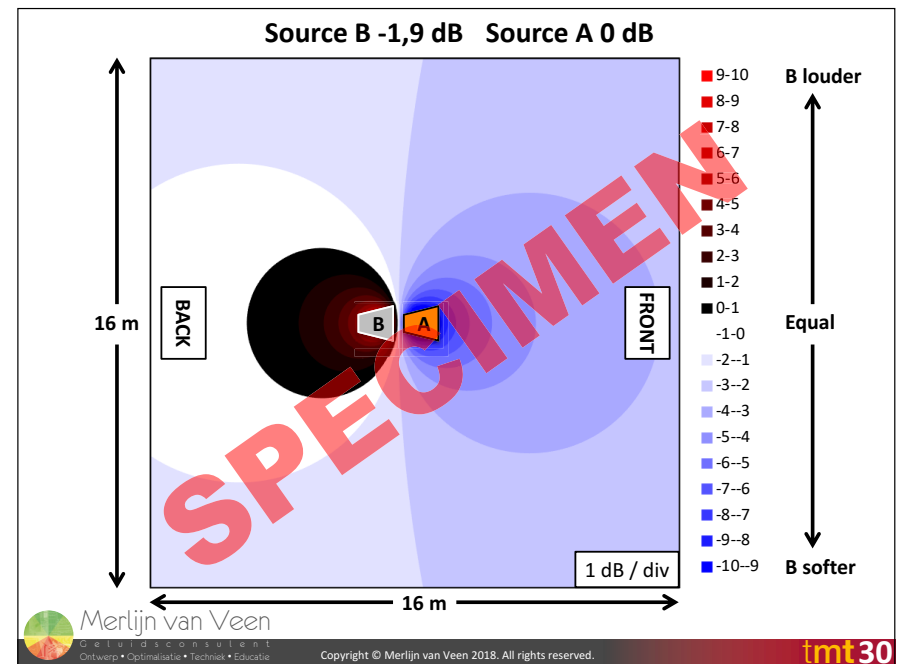
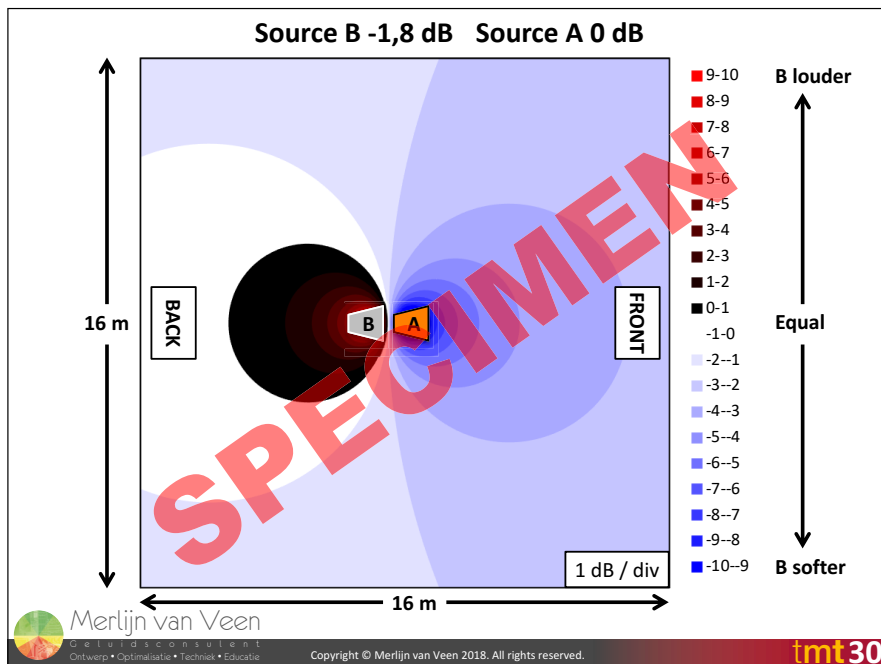
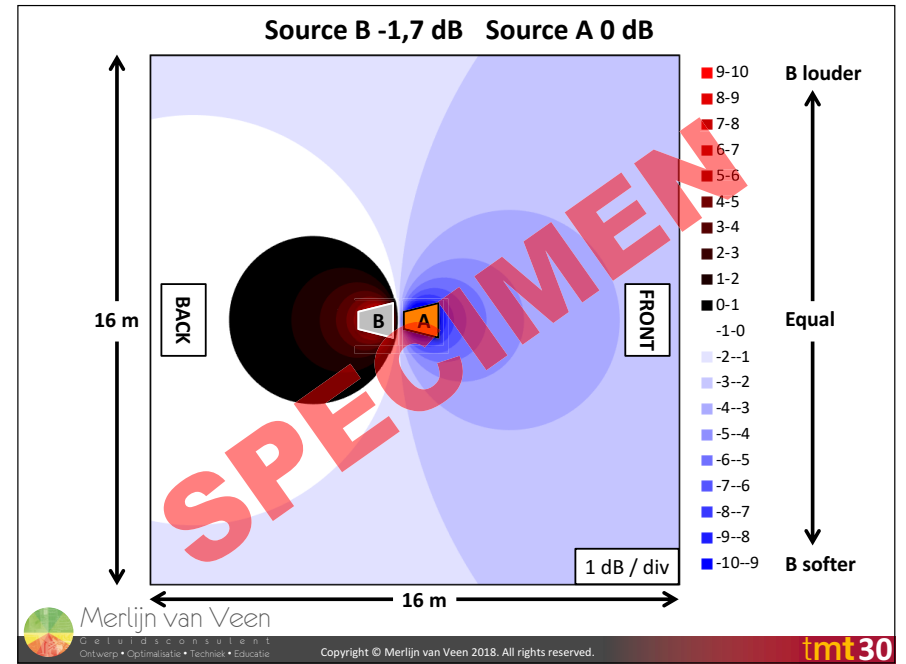
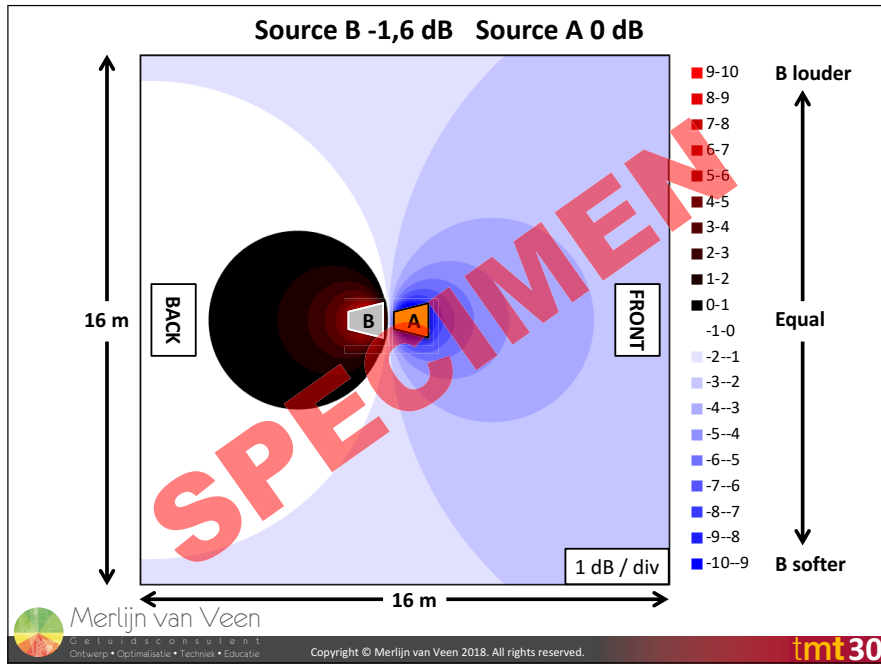


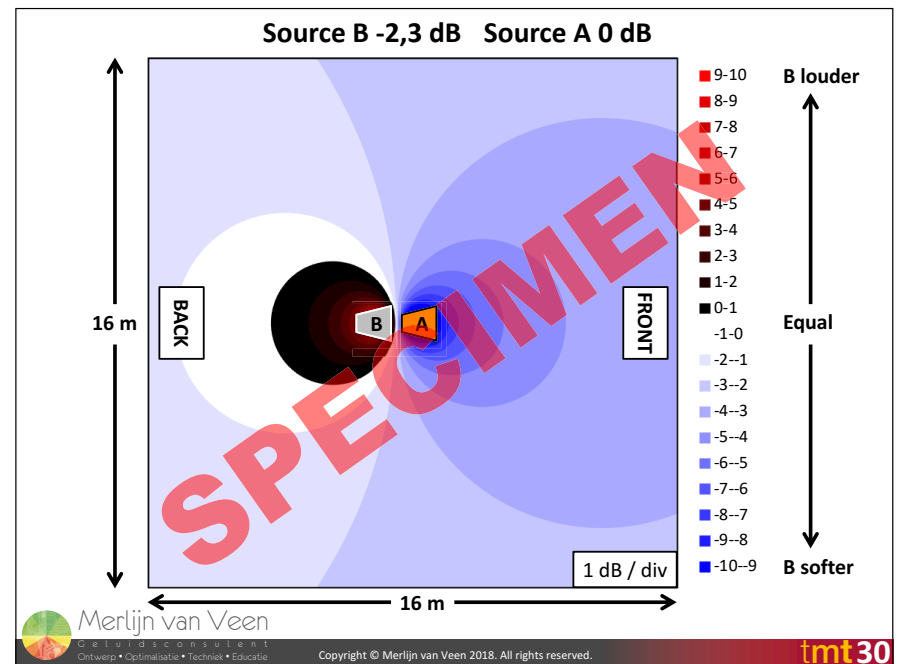
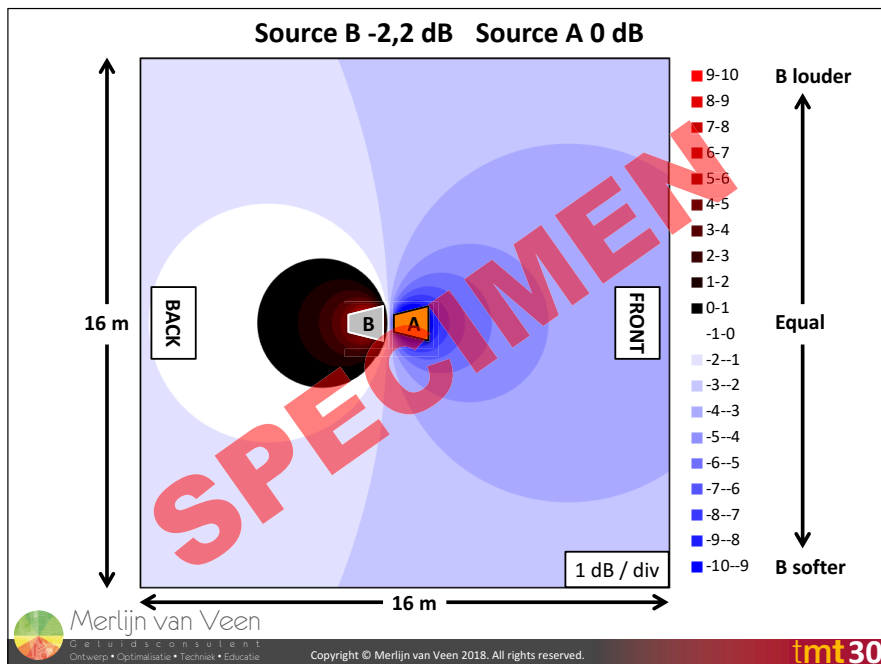
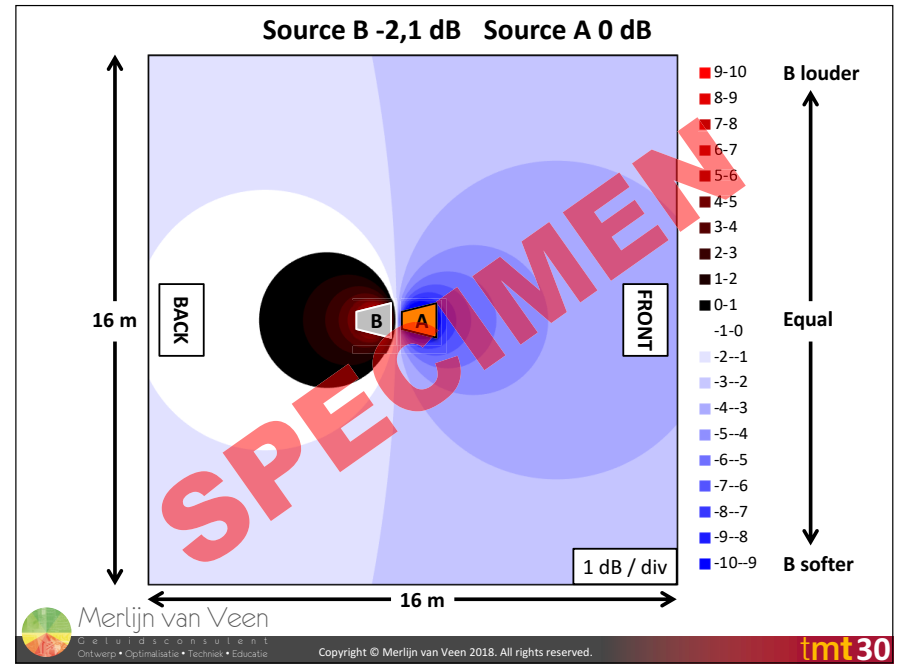
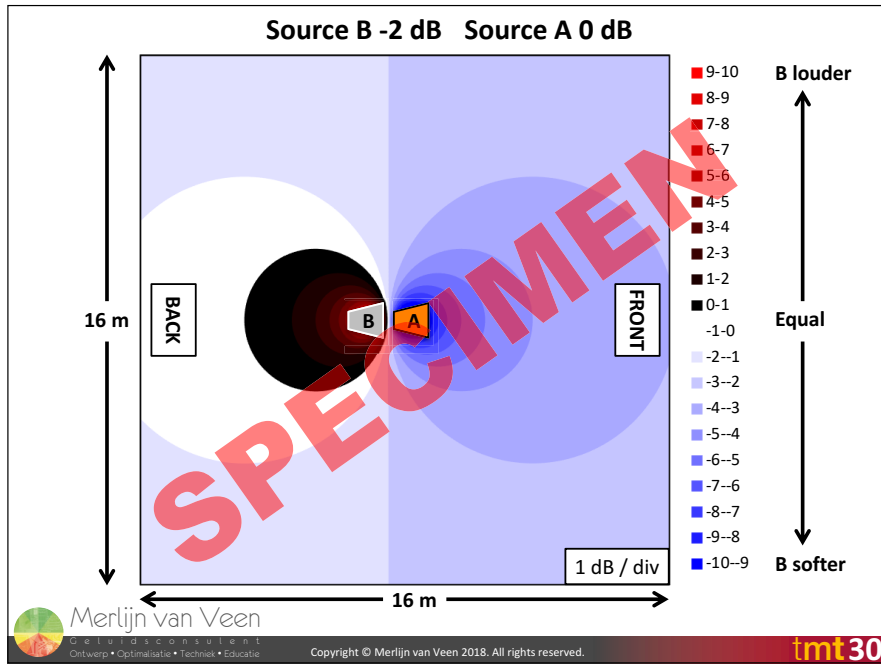


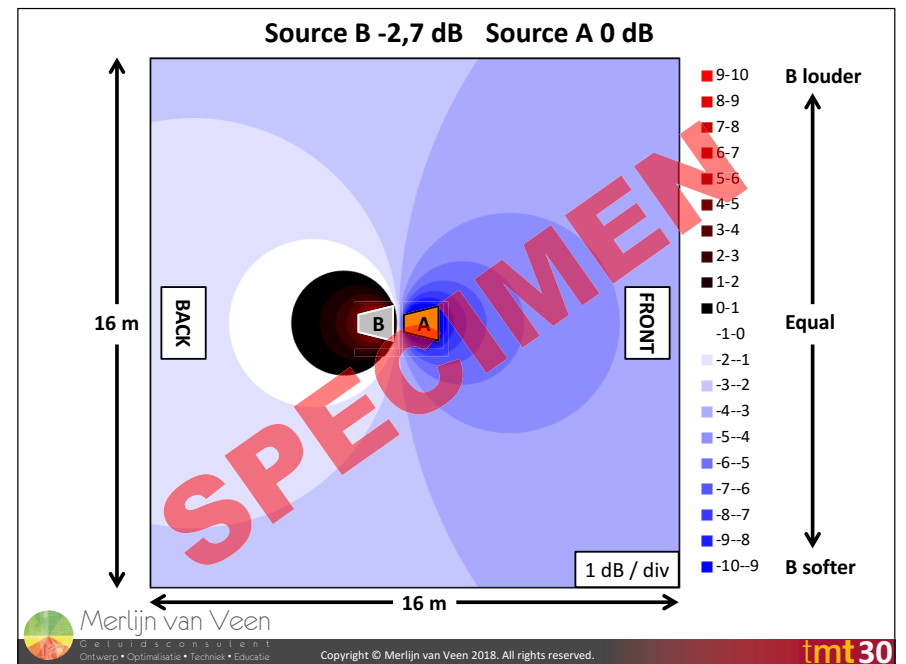
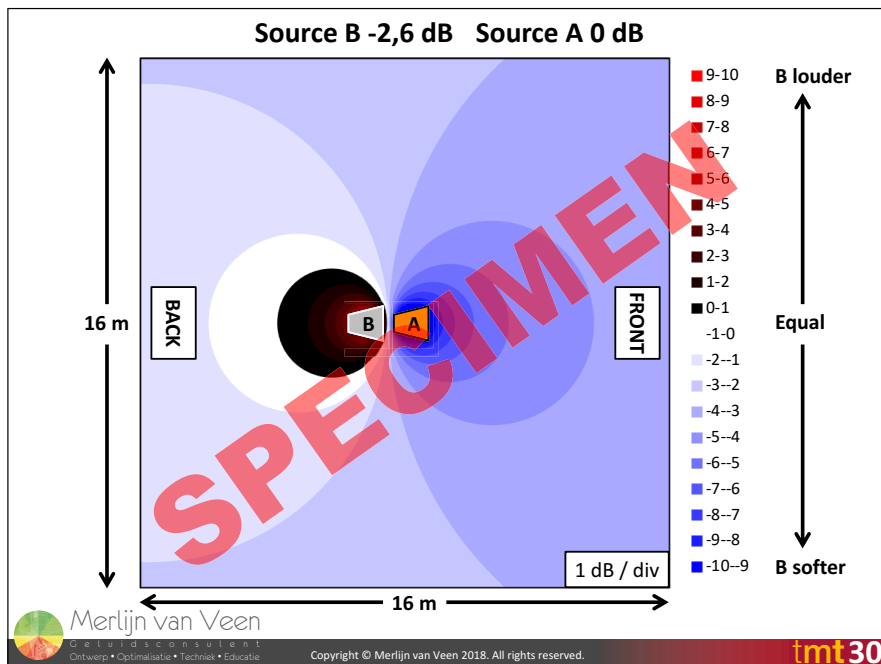
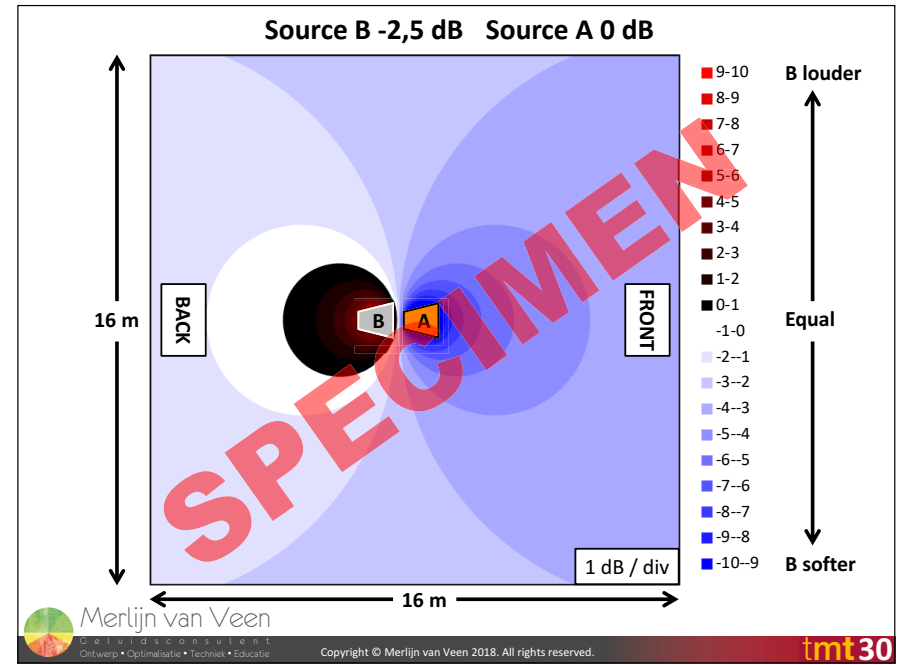
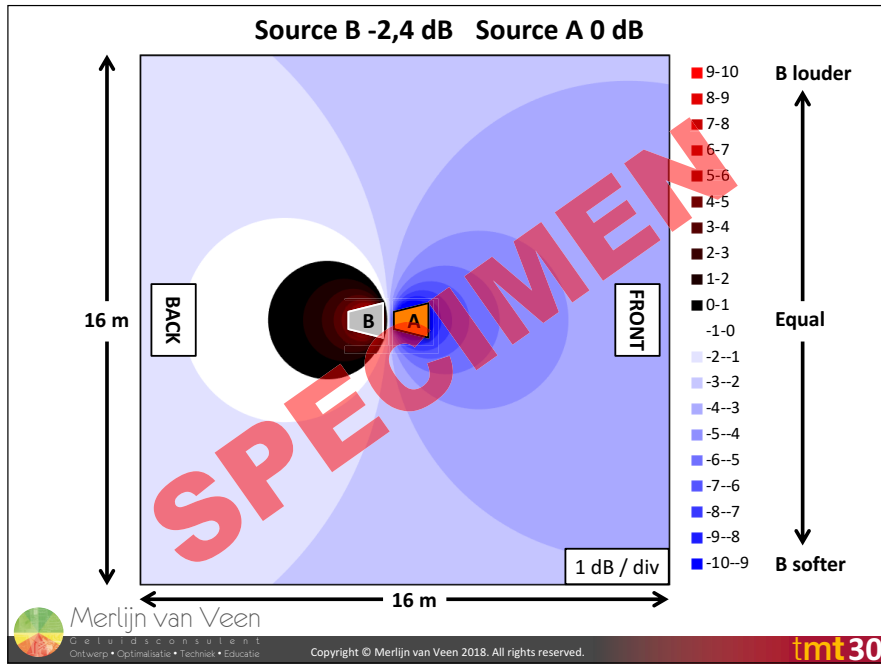


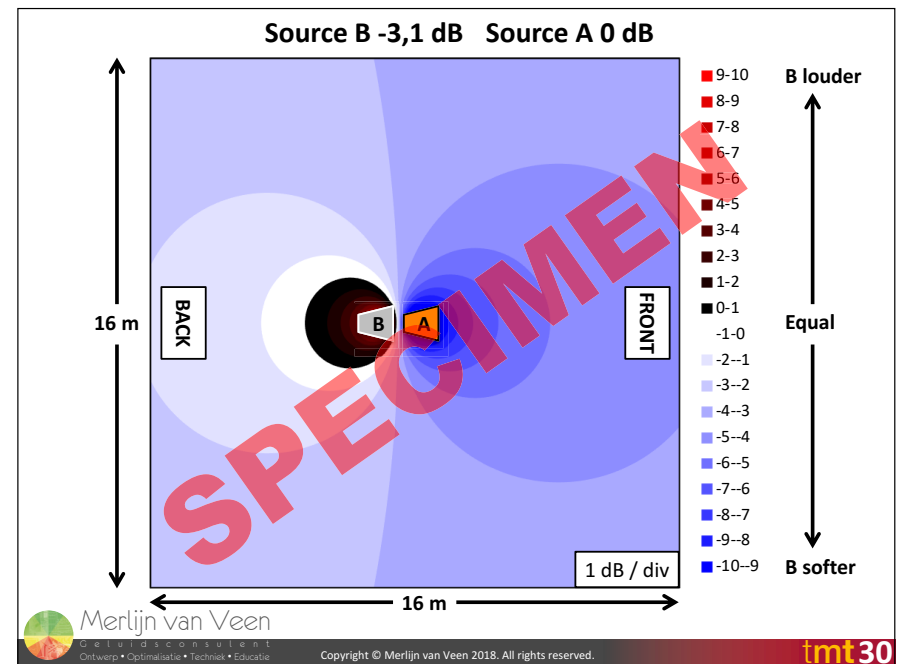
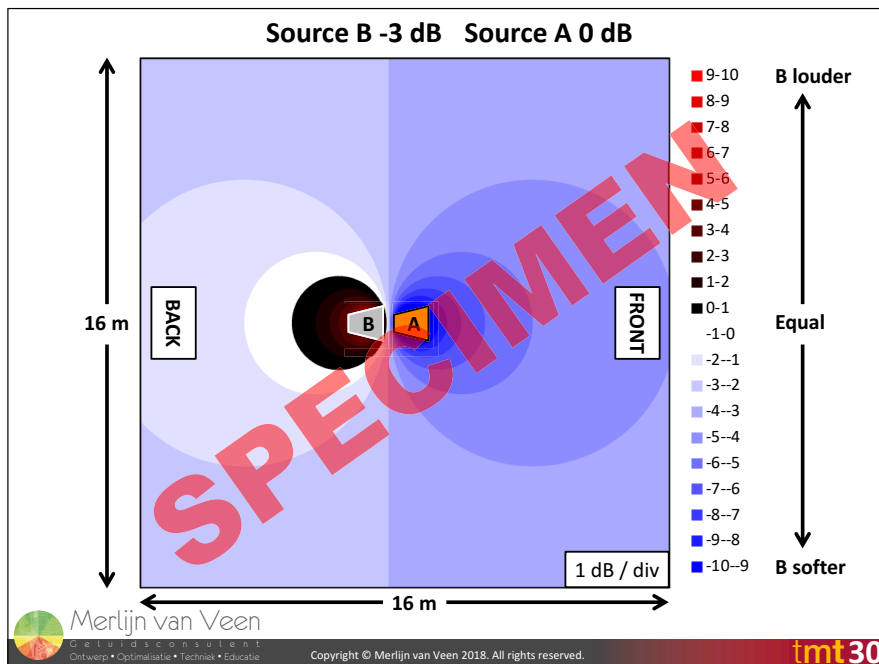
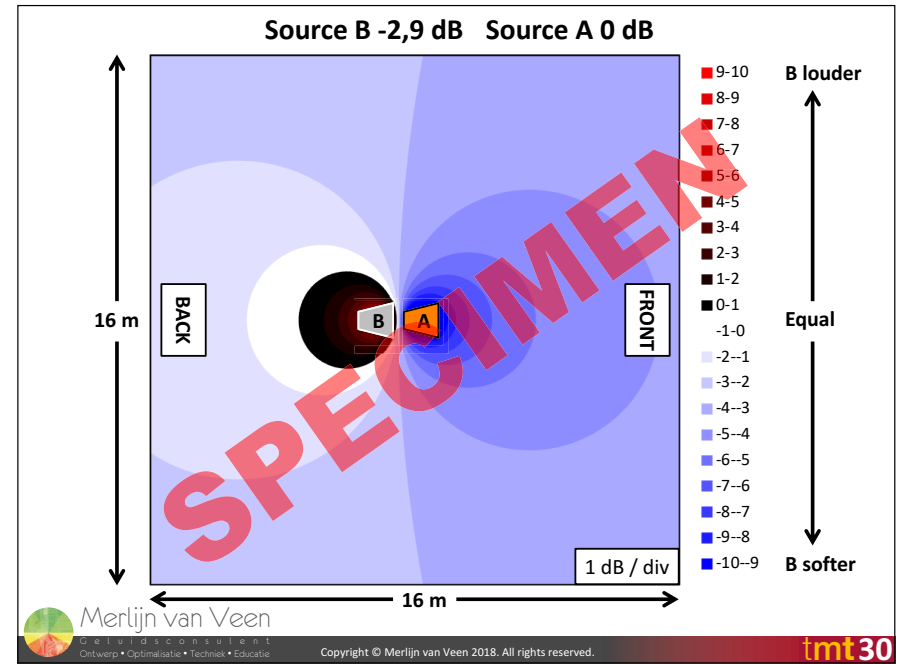
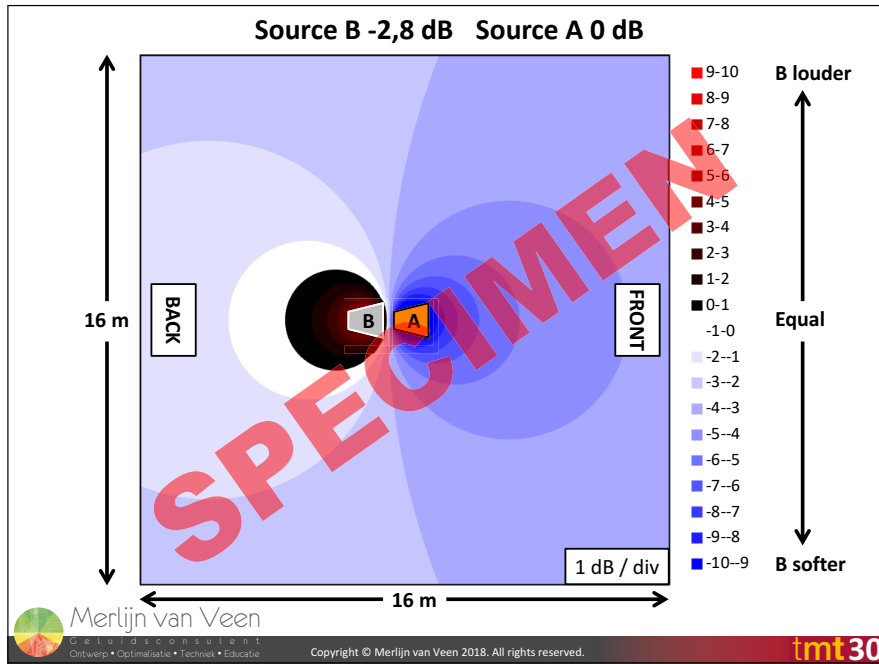


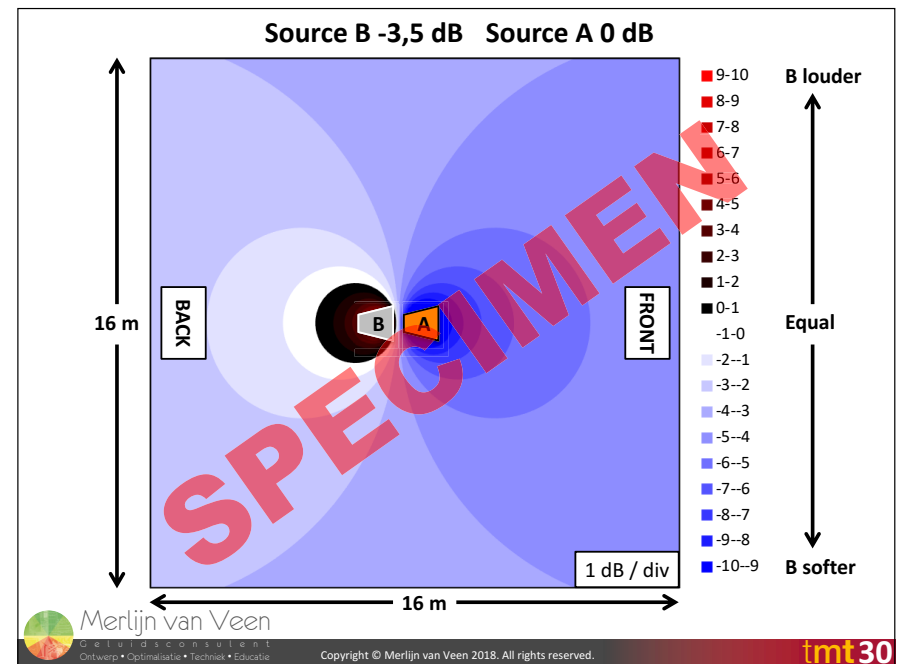
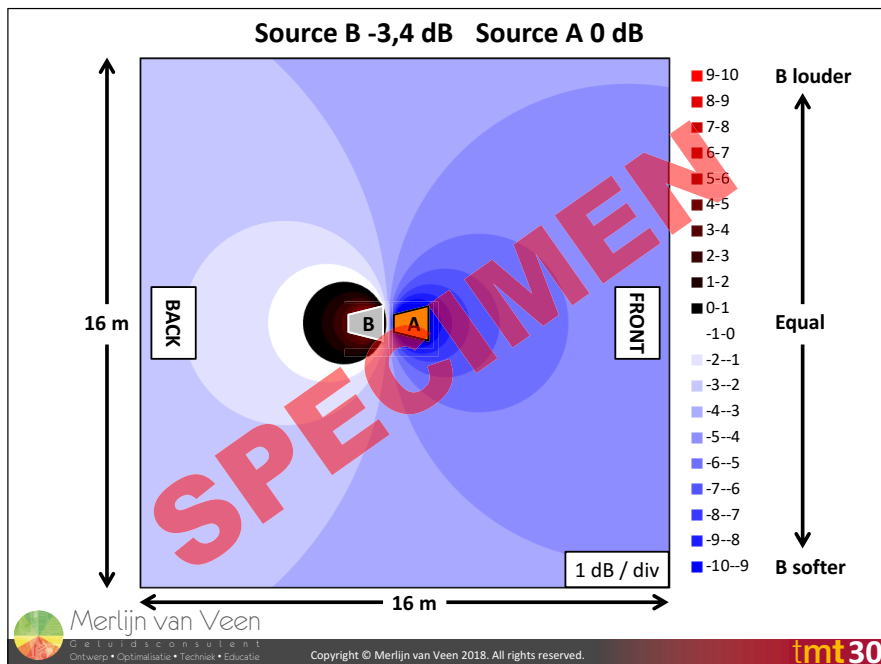
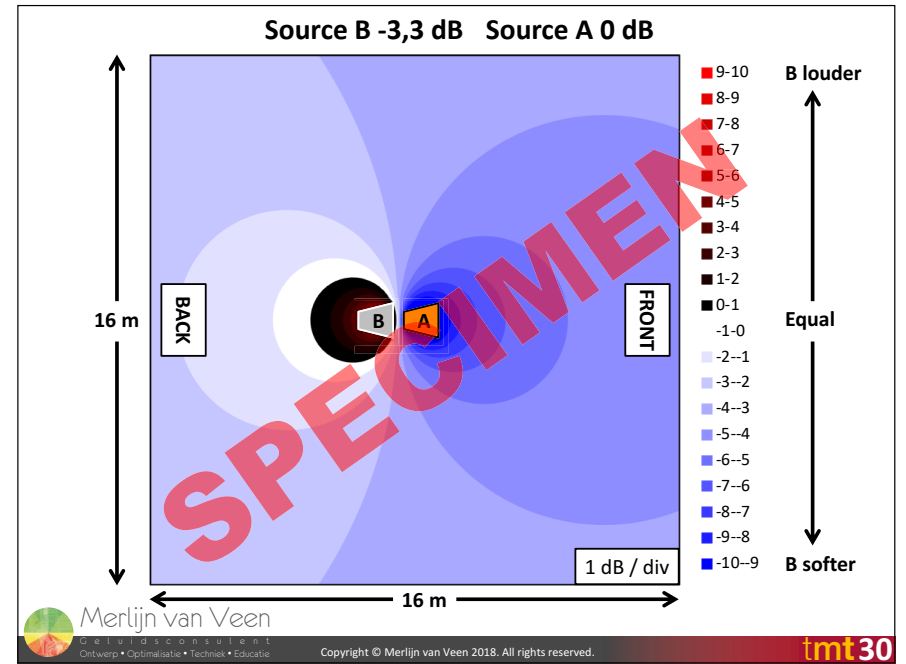
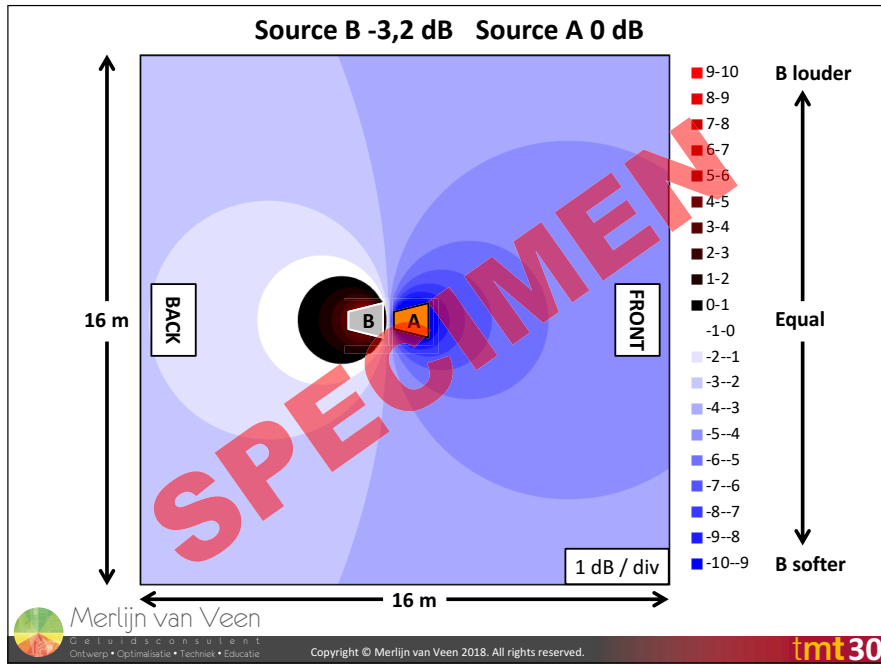


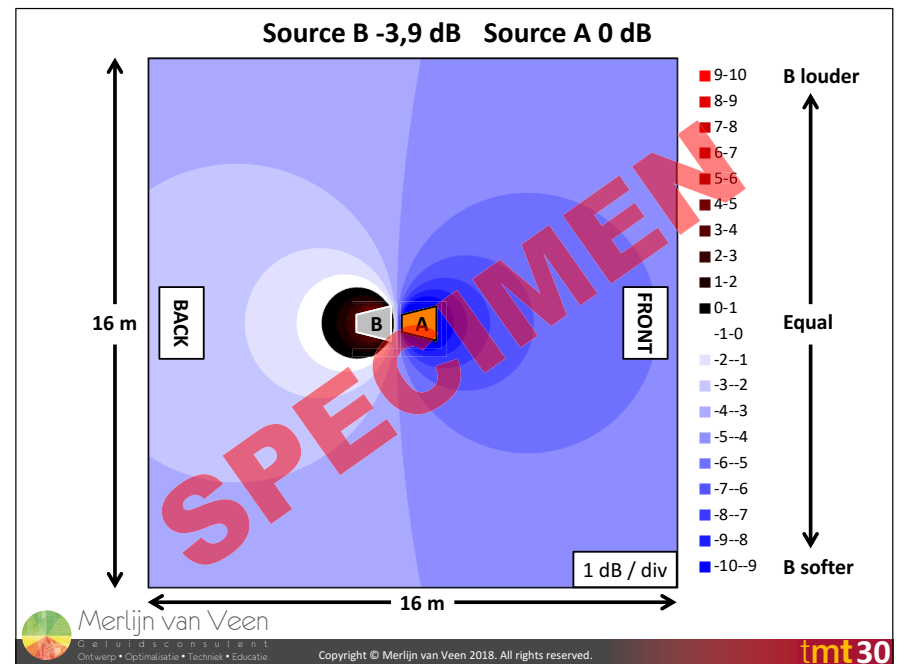
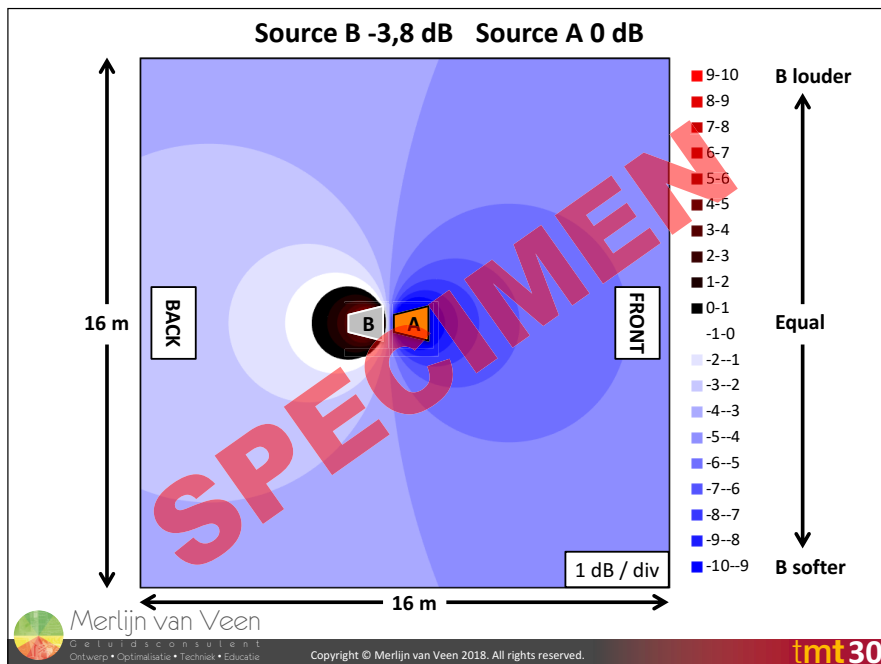
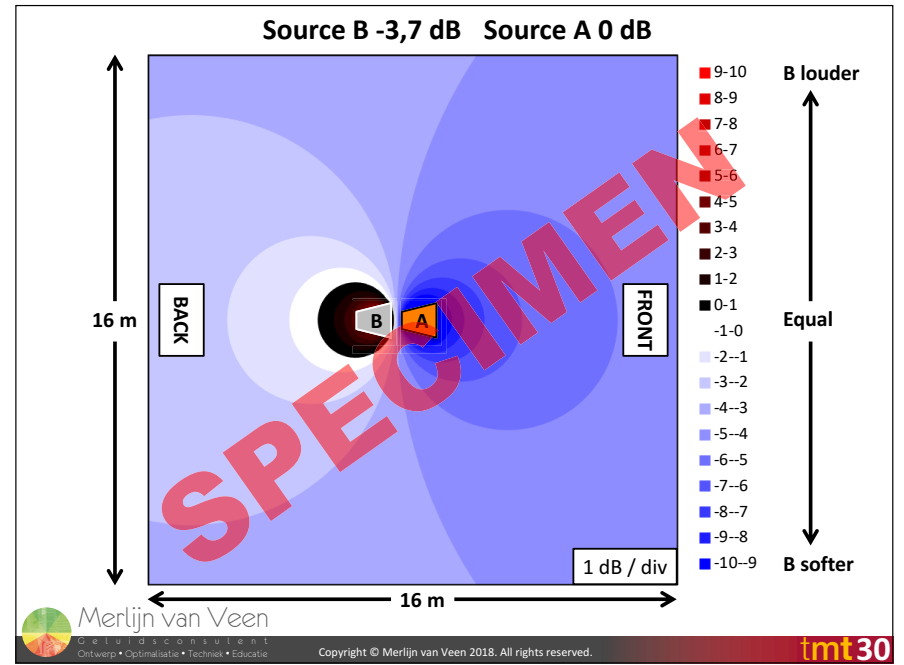
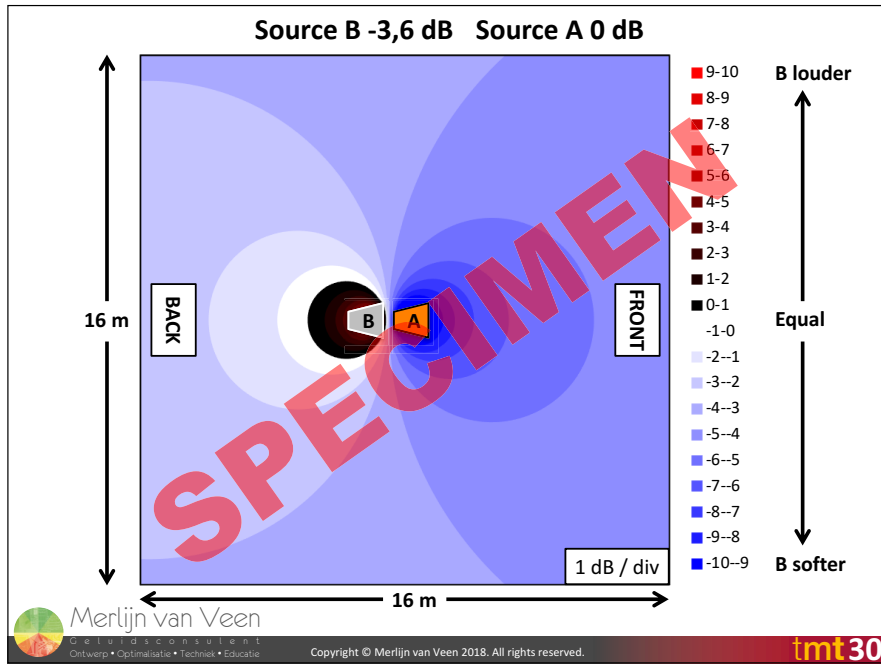


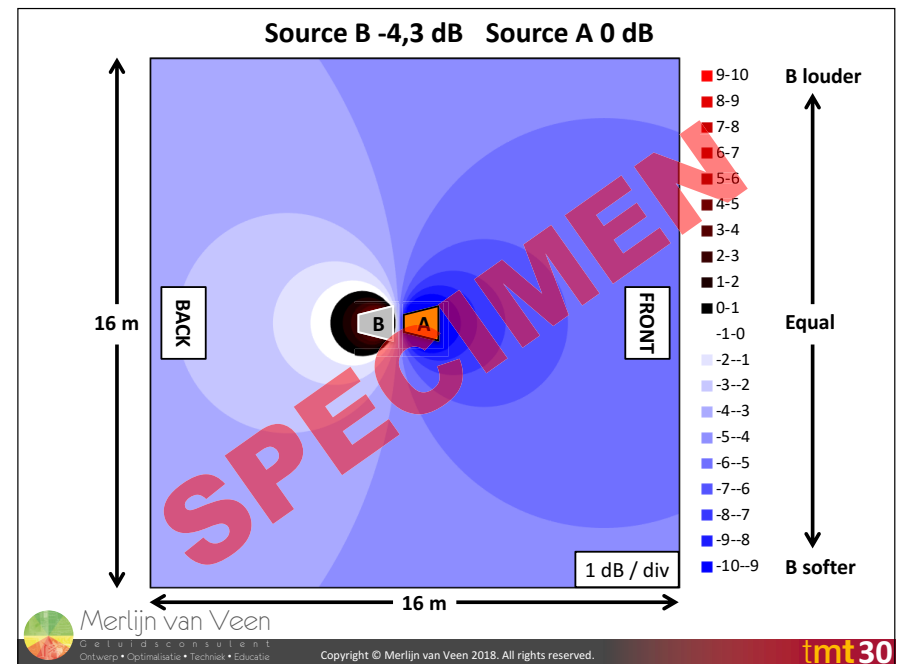
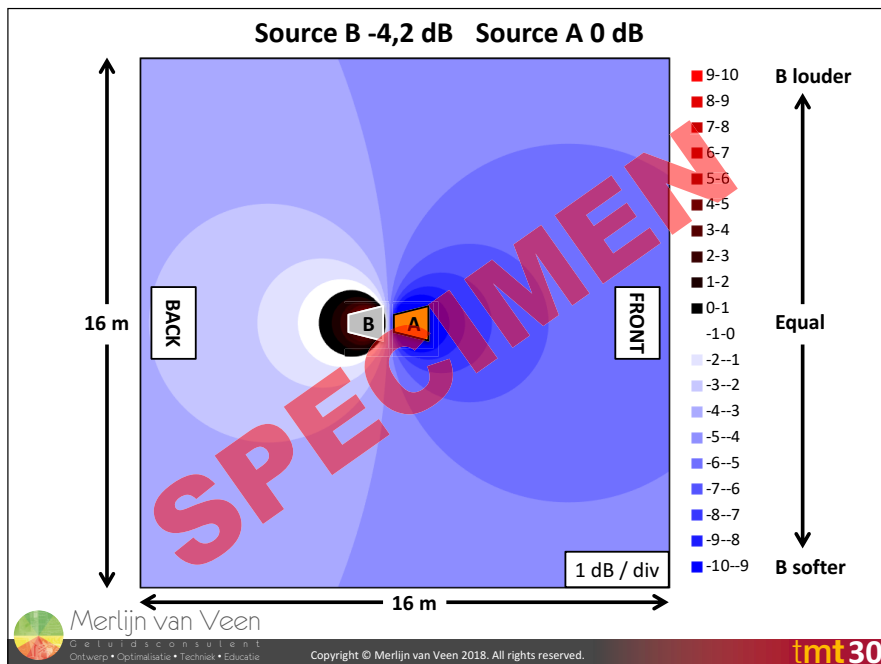
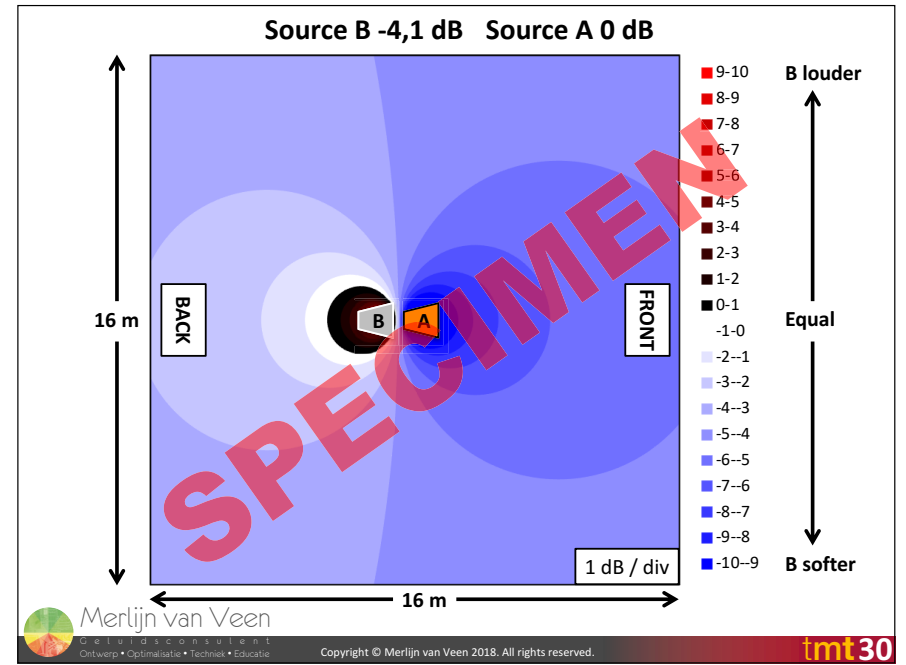
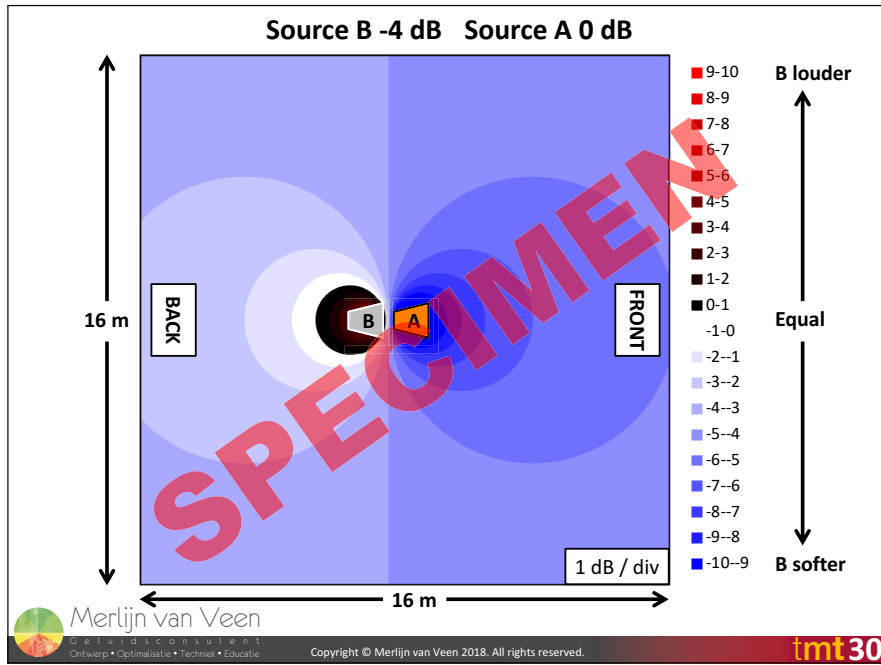


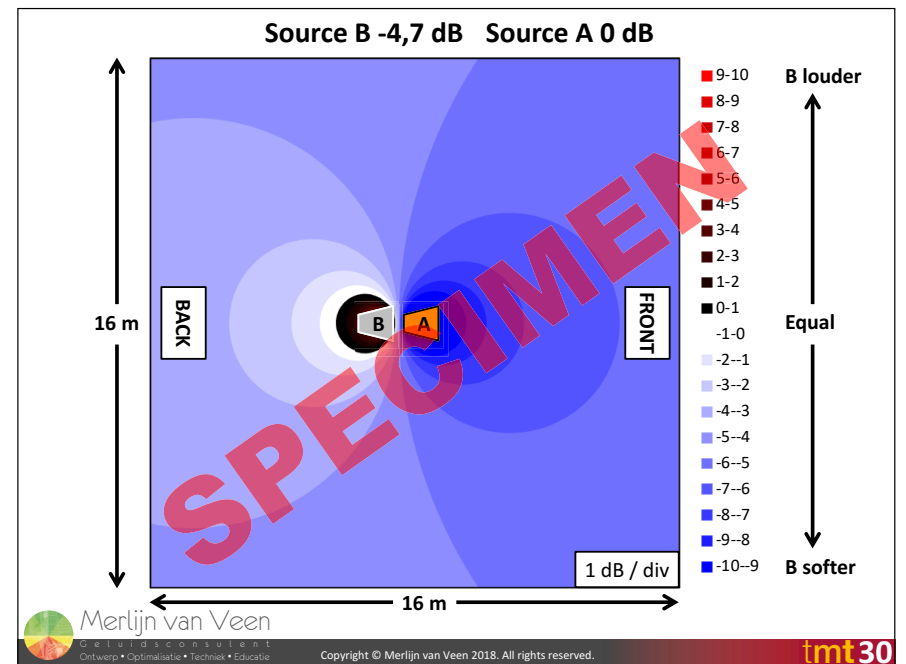
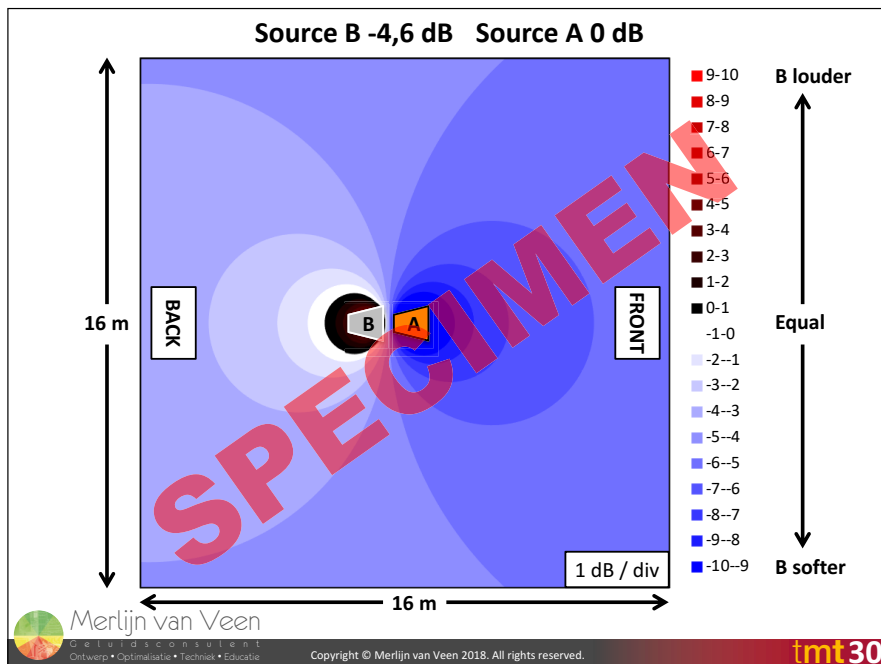
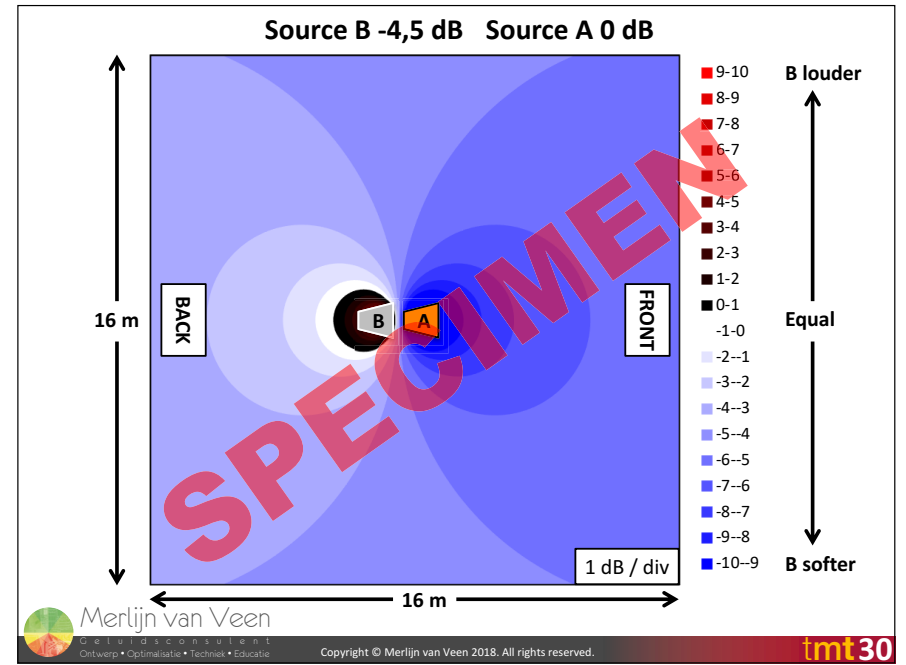
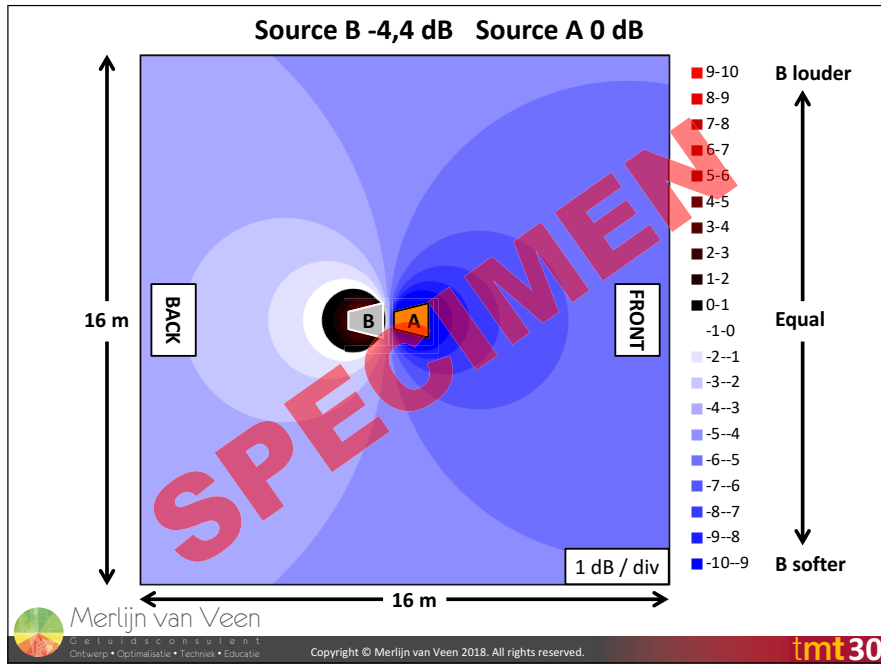


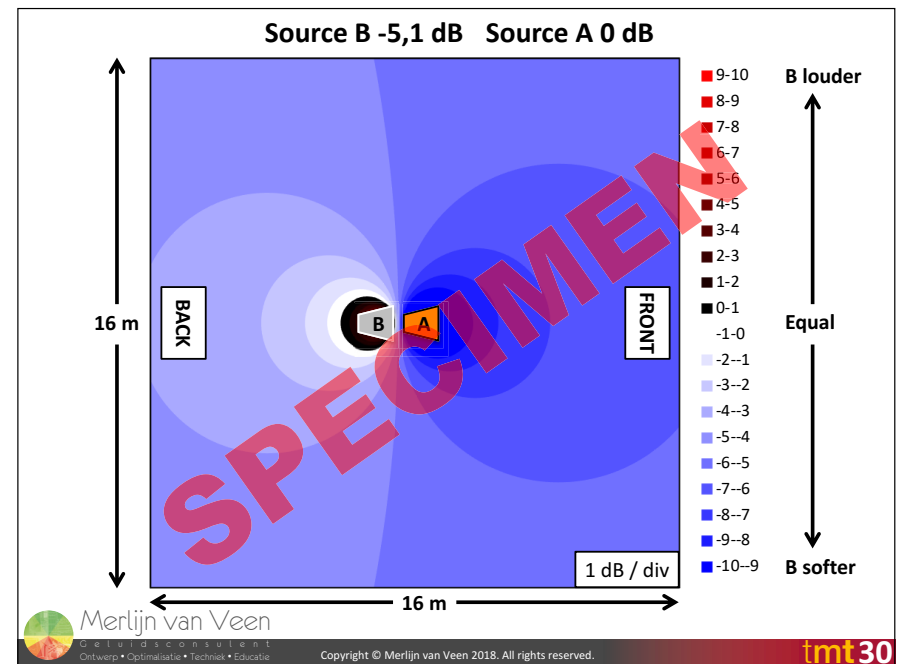
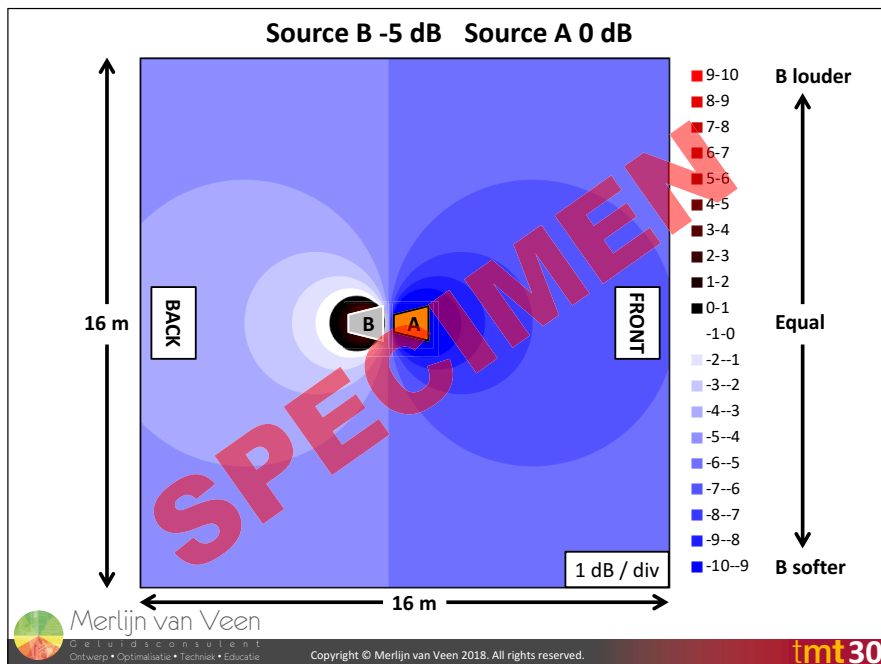
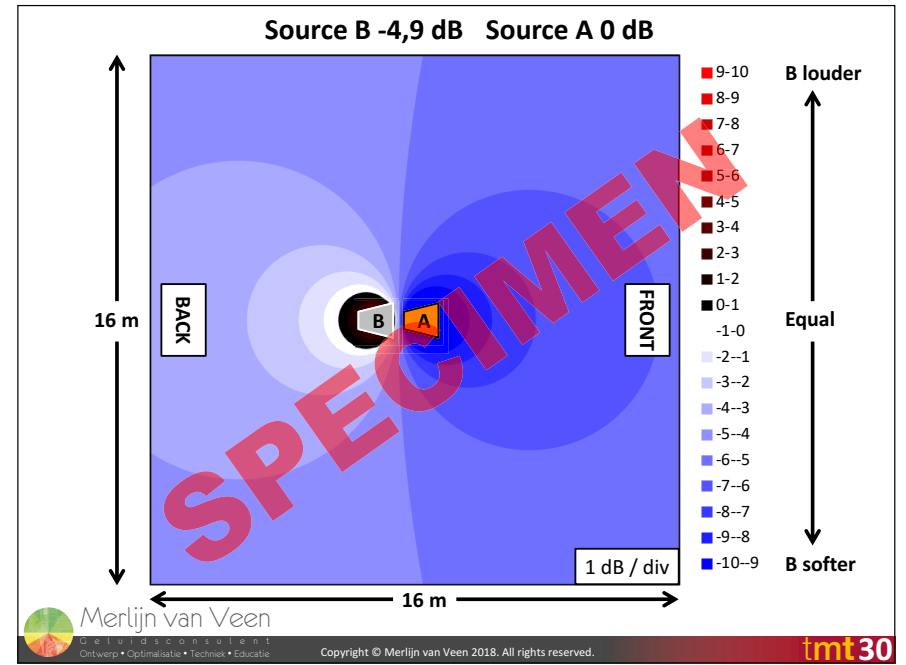
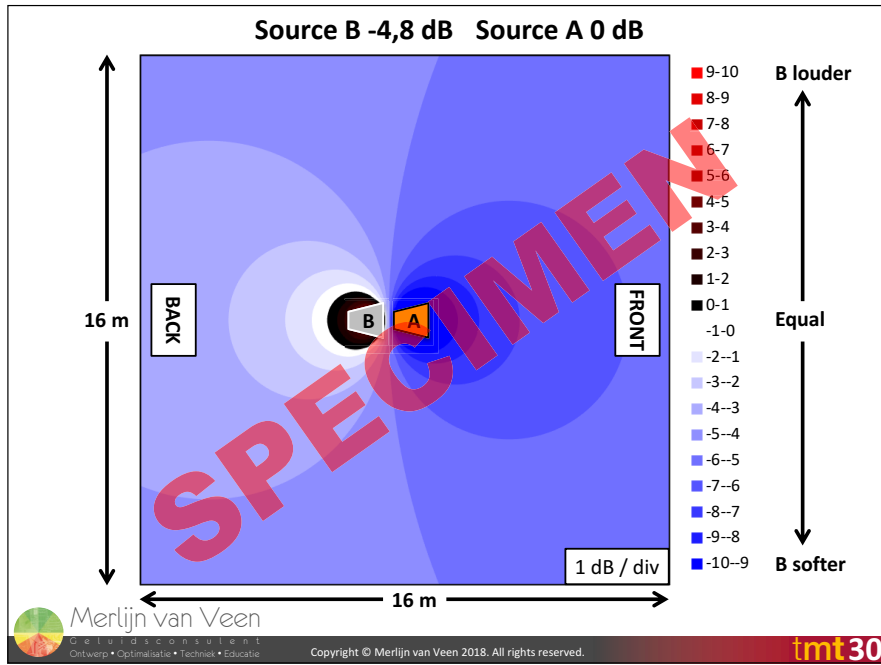


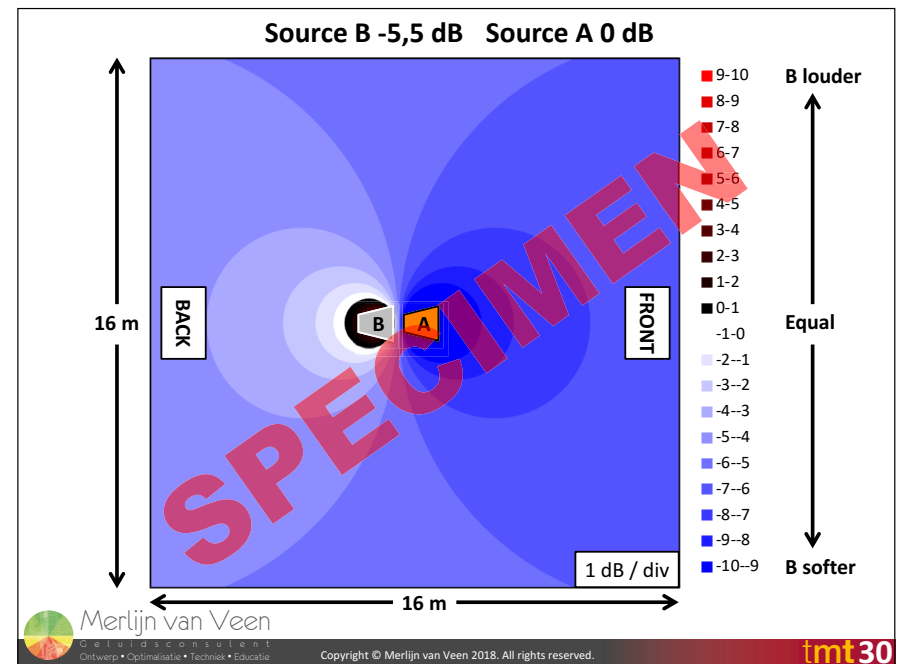
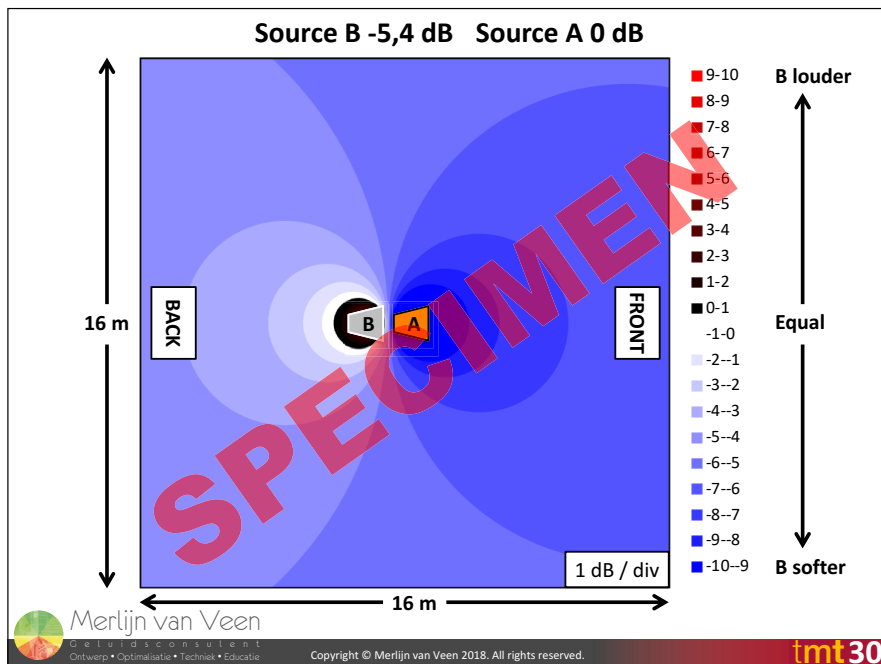
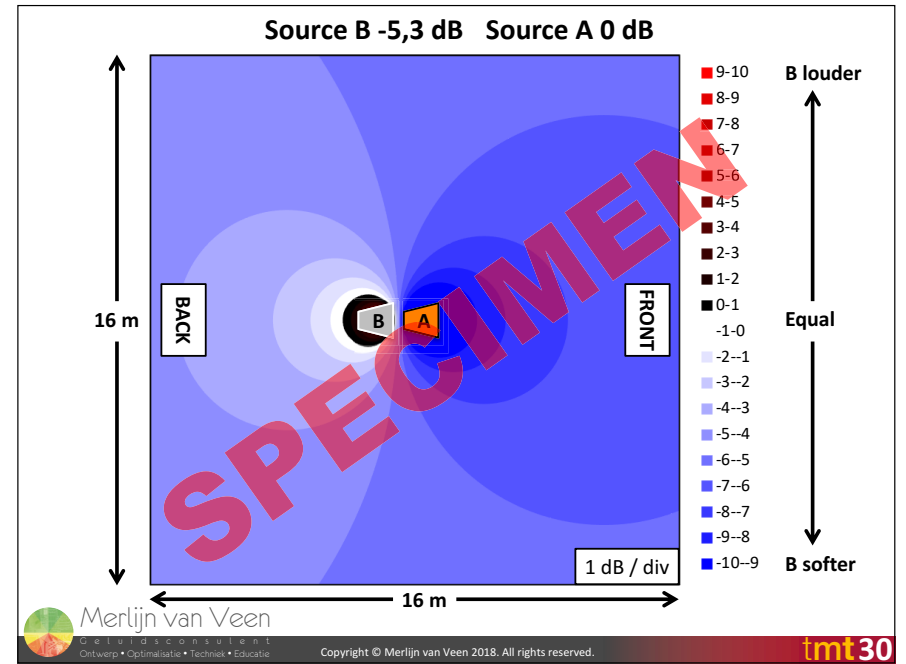
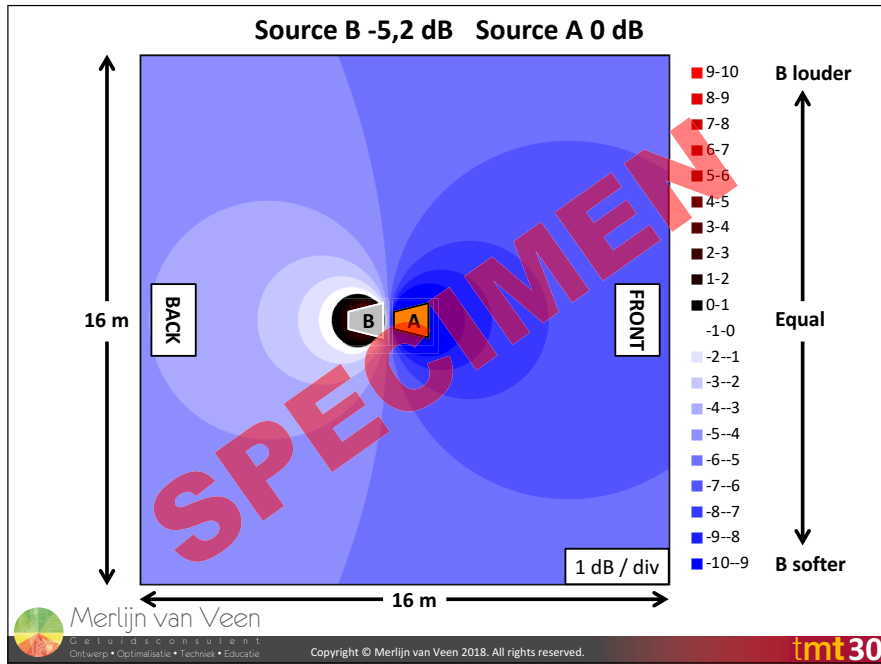


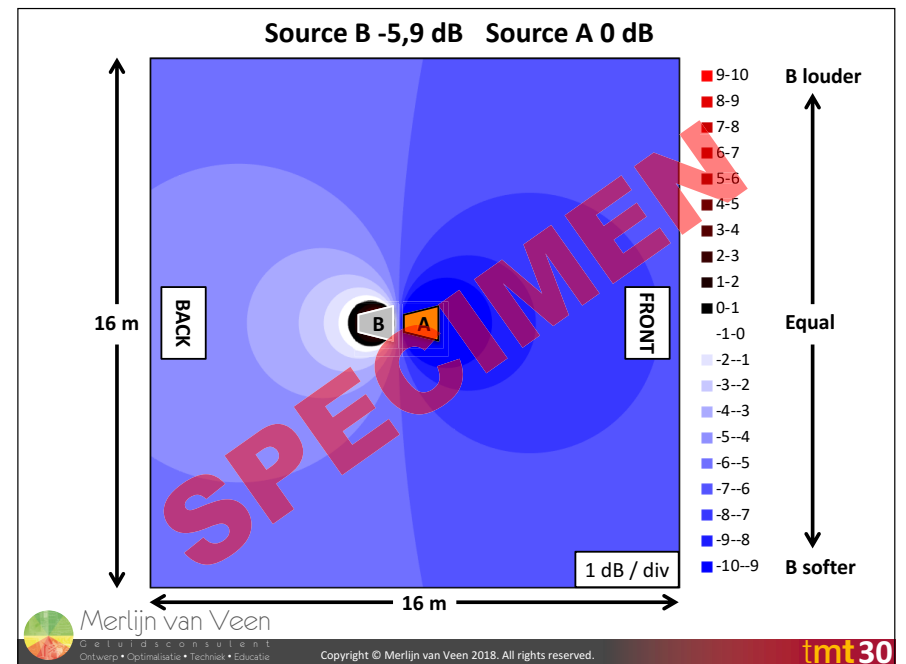
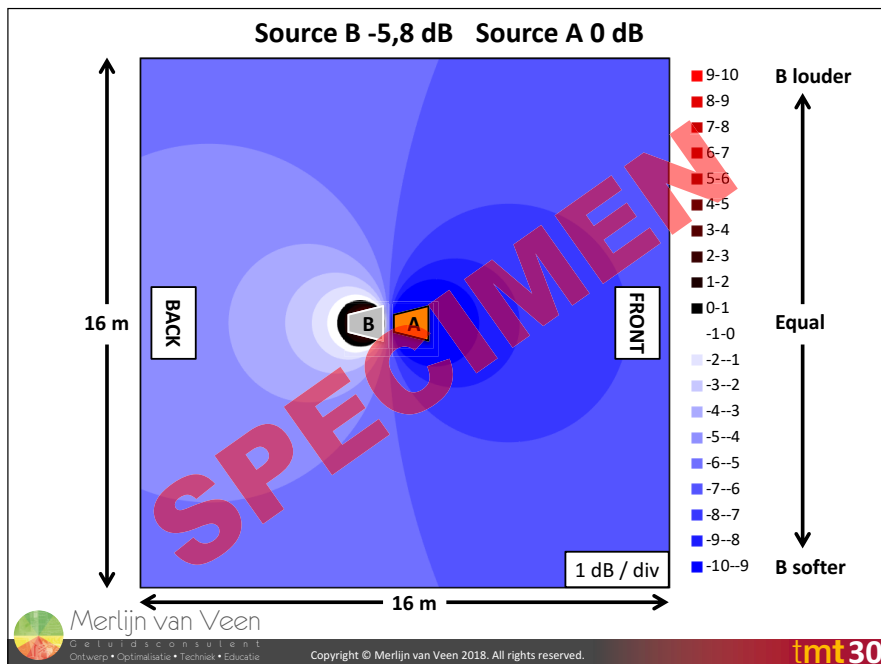
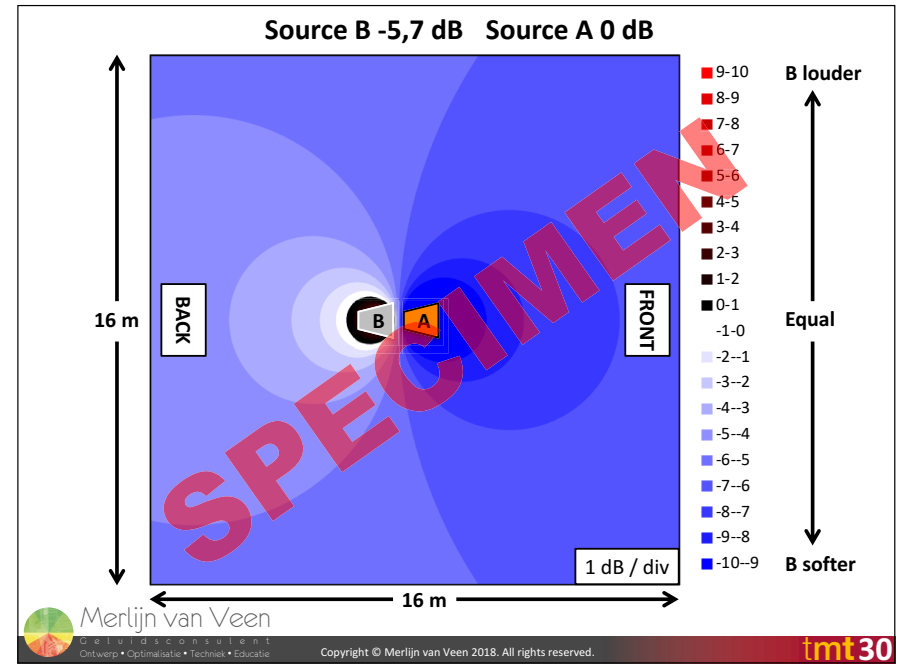
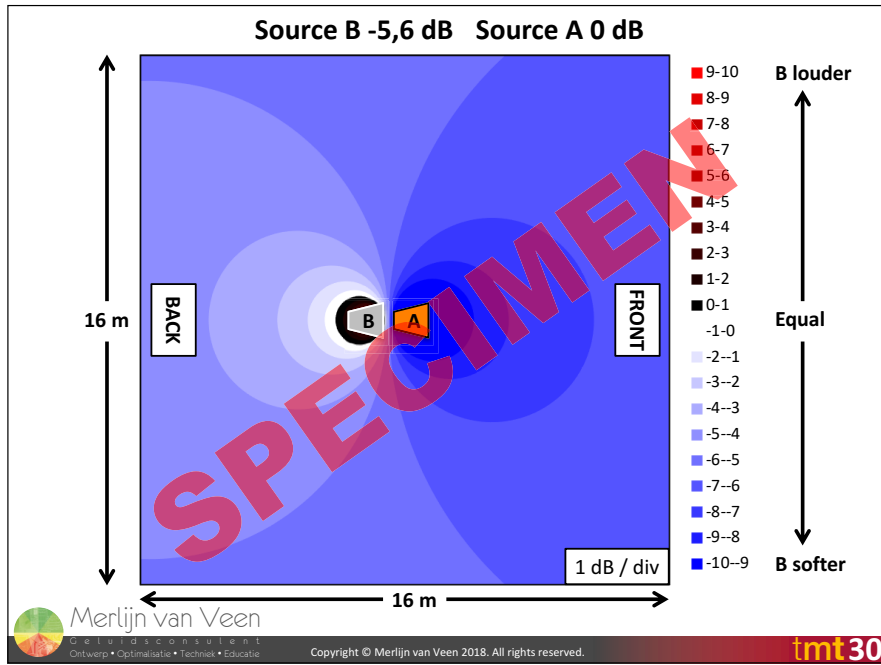


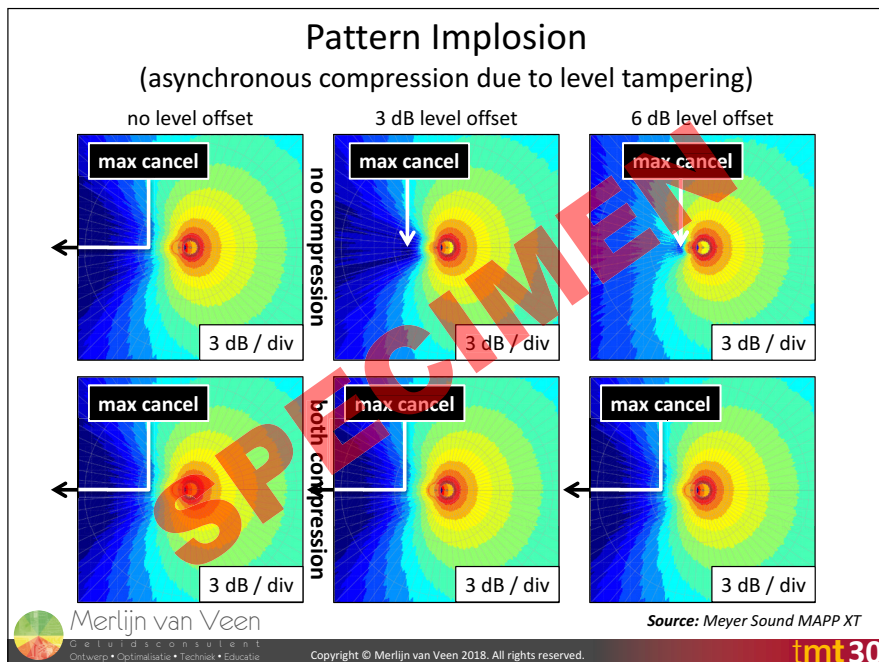
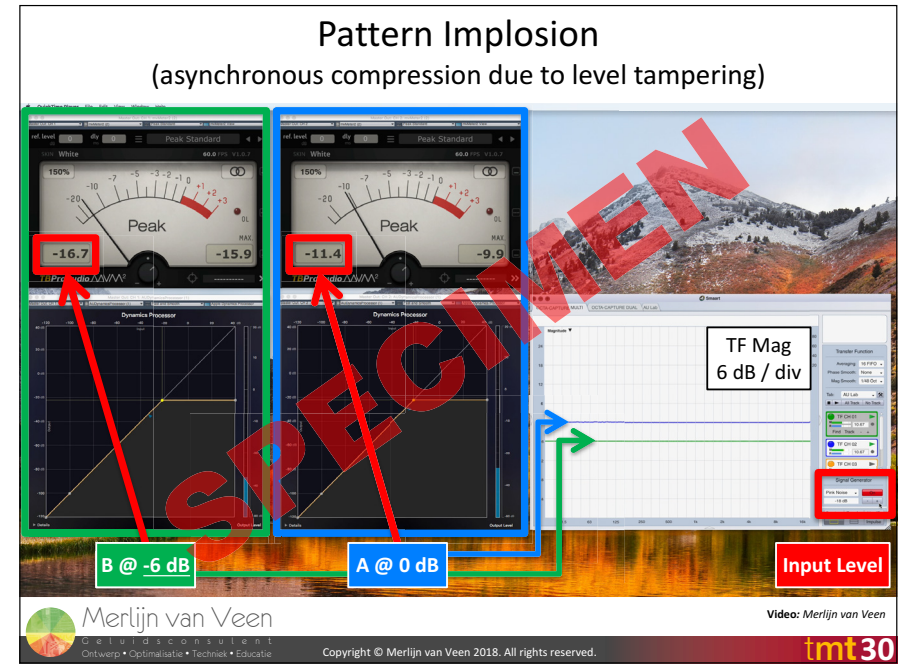
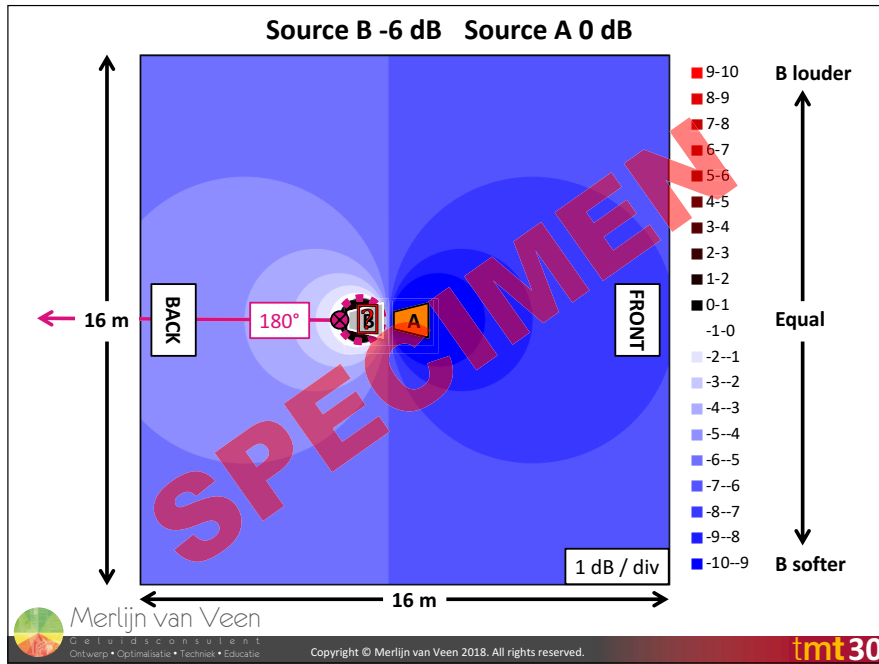












Rules of the Game

- Factory Recommended Loudspeaker Presets*
- Only Delay
- Polarity \emptyset
- No additional processing

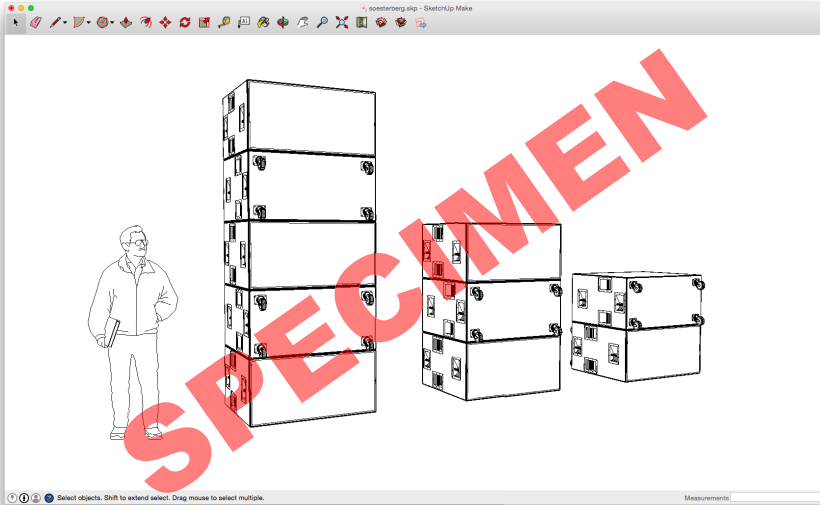
* If applicable

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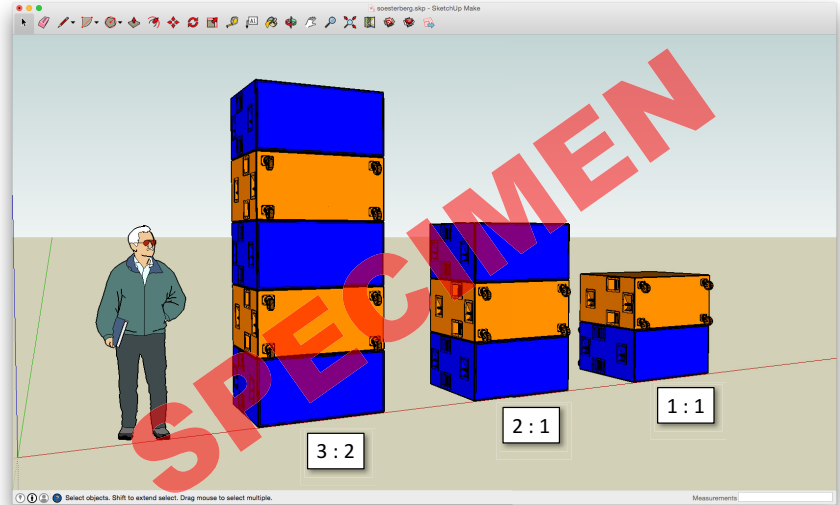
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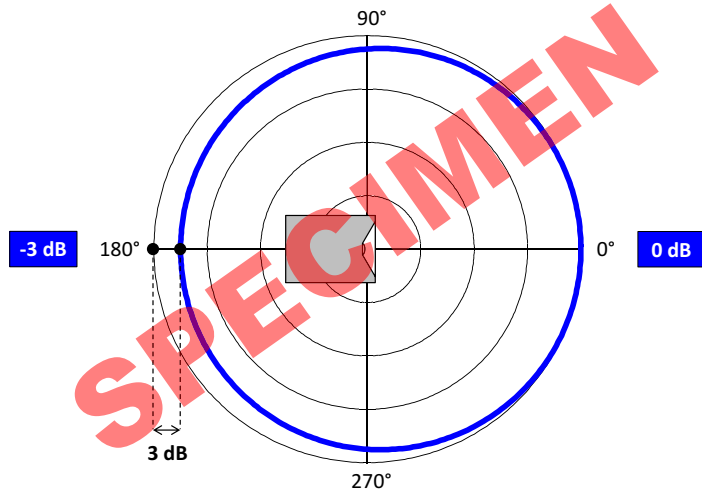
Inverted Stack Gradient - Ratio



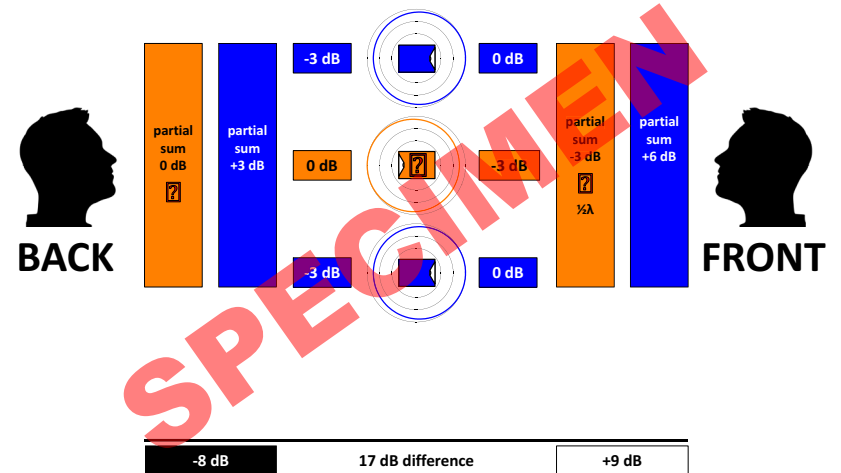
Inverted Stack Gradient - Ratio

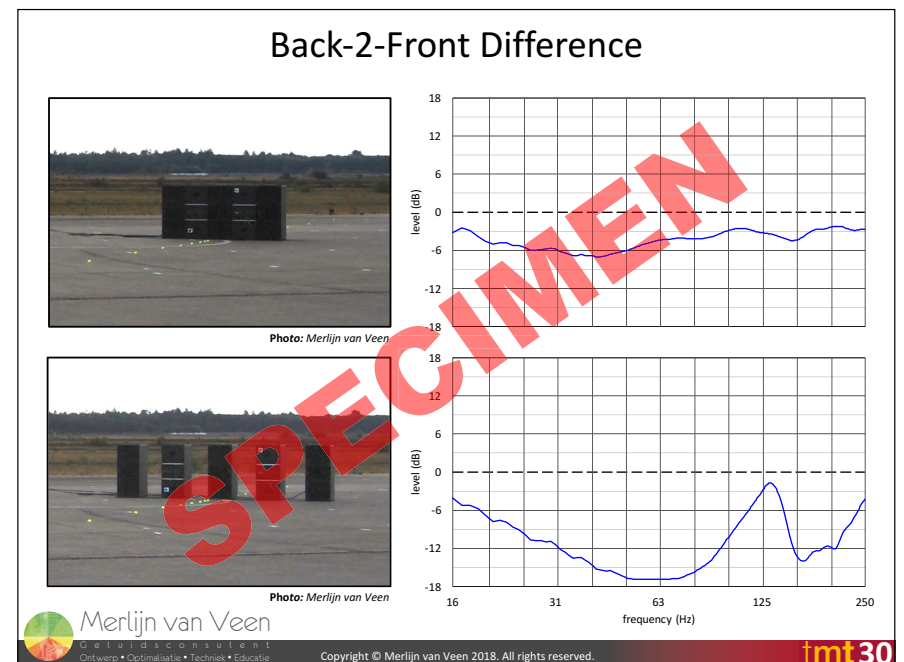
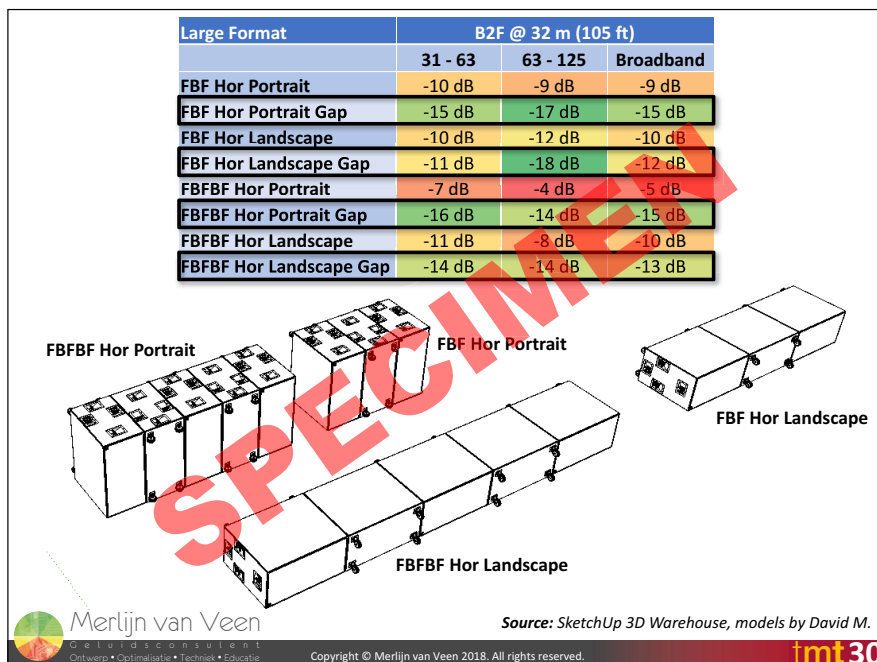
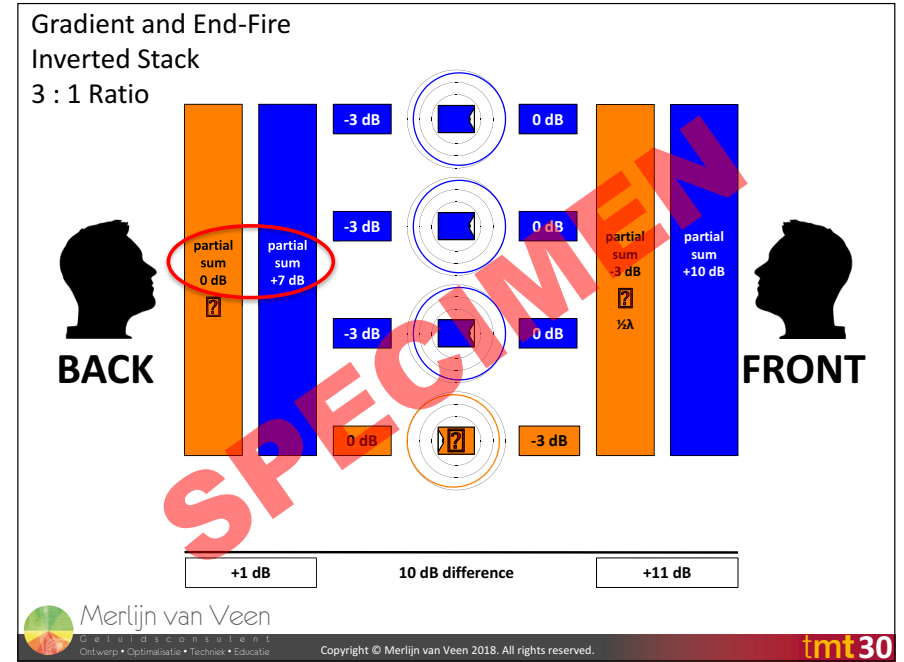
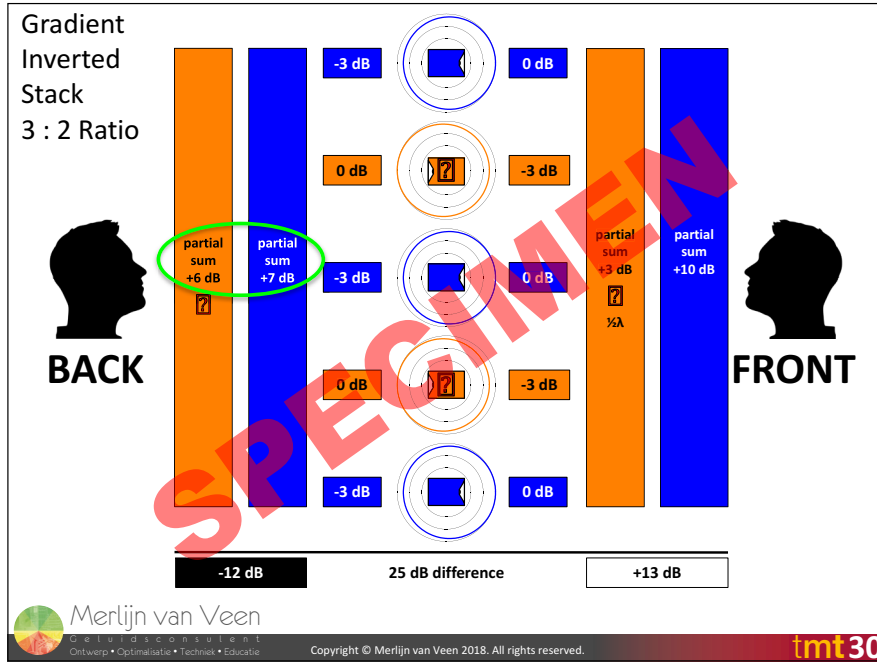


Polar Plot (6 dB / div)



Gradient Inverted Stack – 2 : 1 Ratio





John Vanderkooy

BEng, PhD (McMaster) – Distinguished Professor Emeritus



Photo: erc.org

2010

* **DISCLAIMER:** Research limited to sealed and vented enclosures only

"The Low-Frequency Acoustic Centre: Measurement, Theory and Application"

by John Vanderkooy

Measurements



Analytic proof

$$p(r,t) = \iint [\rho \dot{u}_n(r_{s,t}-R_c) / 4\pi R] dS + \iint [e_n \cdot n_s (\partial/\partial t + c/R) p(r_{s,t}-R_c) / 4\pi R] dS, \quad (1)$$

$$p(r,t) = S(t-r/c)/r - \nabla D(t-r/c)/r + \sum (\partial^2/\partial x_p \partial x_q) Q_{pq}(t-r/c)/r + \dots, \quad (2)$$

$$S(t) = (\rho/4\pi) \iint \dot{u}_n(r_{s,t}) dS, \quad (3)$$

$$D(t) = (1/4\pi) \iint [\rho r_s \dot{u}_n(r_{s,t}) + n_s p(r_{s,t})] dS, \quad (4)$$

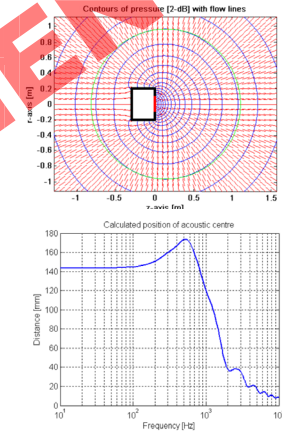
$$Q_{pq}(t) = (1/8\pi) \iint [\rho x_{sp} x_{sq} \dot{u}_n(r_{s,t}) + (x_{sp} n_q + x_{sq} n_p) p(r_{s,t})] dS, \quad (5)$$

$$0 = \iint [\rho (r_s - r_0) \dot{u}_n(r_{s,t}) + n_s p(r_{s,t})] dS, \quad (6)$$

$$\iint r_0 \dot{u}_n(r_{s,t}) dS = r_0 A(t), \quad (7)$$

$$r_0 = (1/A) \iint [r_s \dot{u}_n(r_{s,t}) + n_s p(r_{s,t})/c] dS. \quad (8)$$

Numerical computation (i.e. BEM)

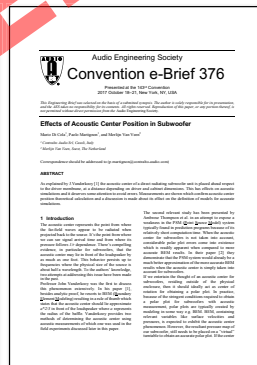
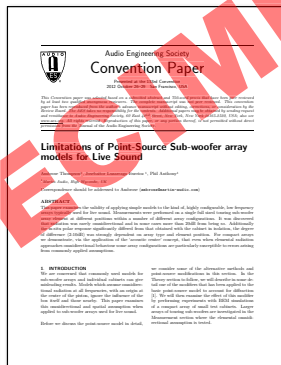
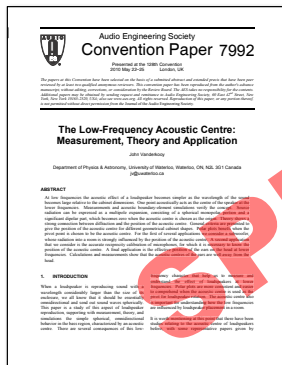


Acoustic Center for LF (Subwoofers)

John Vanderkooy*
2010

Ambrose Thompson et al.
2010

Mario Di Cola et al.
2017

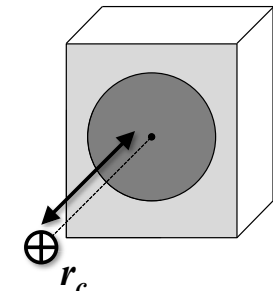


Acoustic Center for LF (Subwoofers)

"The acoustic center represents the point from where the far-field waves appear to emanate when projected back to the source."

It is the point from where we can see:

- pressure follows $1/r$ dependence (inverse-square-law)
- signal arrival time



Acoustic Center for LF (Subwoofers)

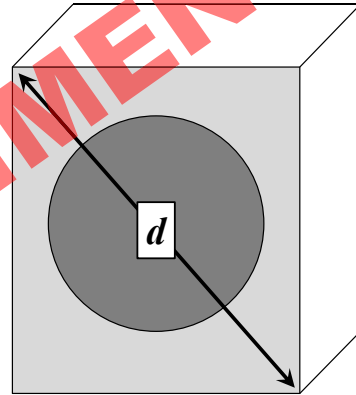
The phenomenon is observed

when

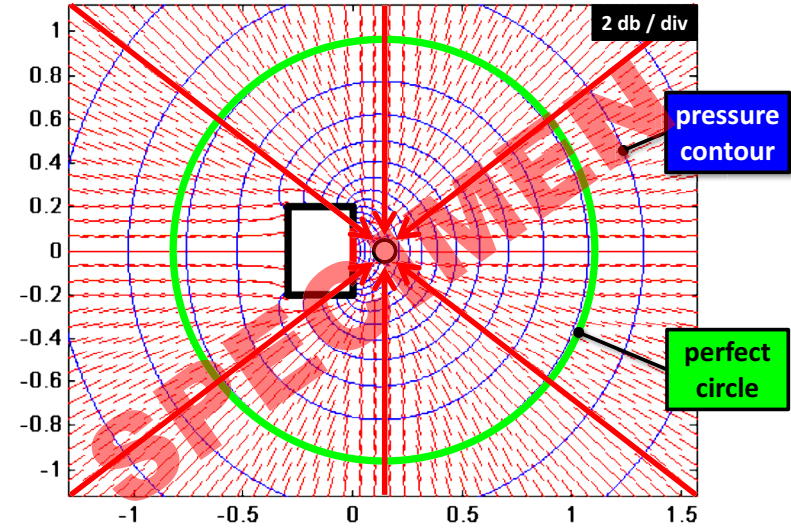
$$f \leq \frac{\text{sound speed}}{2d}$$

or

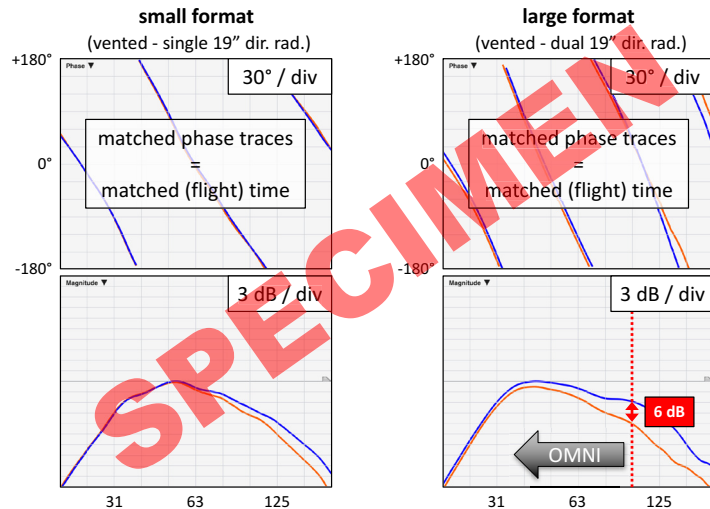
$$d \leq \frac{1}{2}\lambda$$



Pressure contours with flow lines



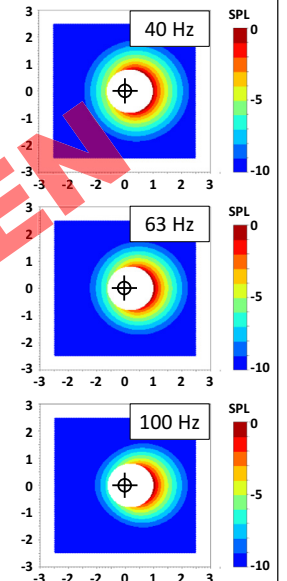
Common live sound subwoofers* are virtually omnidirectional (equitemporal = equidistant)



Near-Field-Scanner (NFS) by Klippel

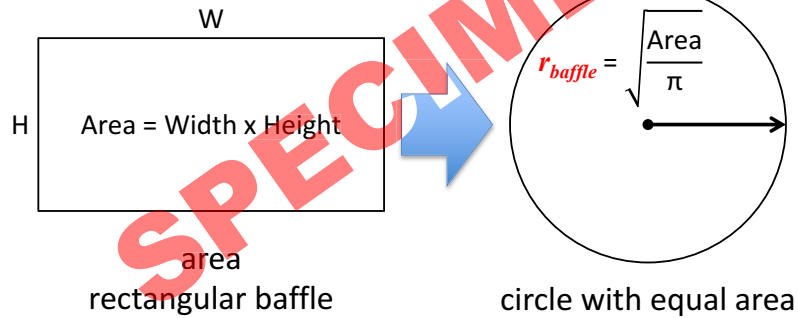


Photo: Klippel.de

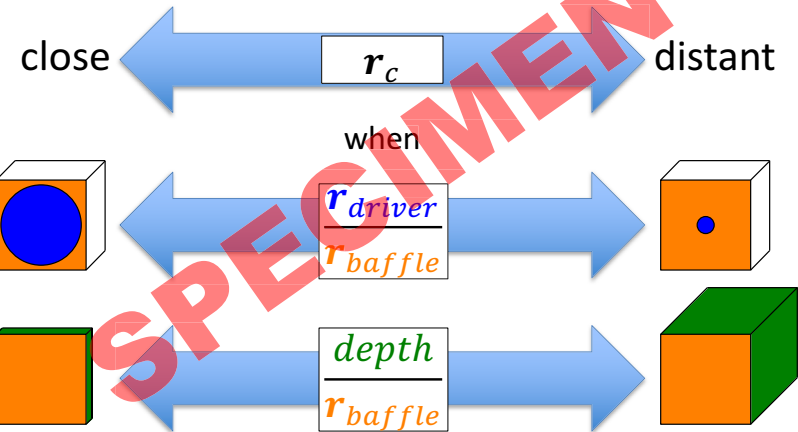


Acoustic Center for LF (Subwoofers)

Limits: $\frac{1}{2} r_{baffle} < r_c < r_{baffle}$
 Rule of thumb: $r_c \approx \frac{2}{3} r_{baffle}$

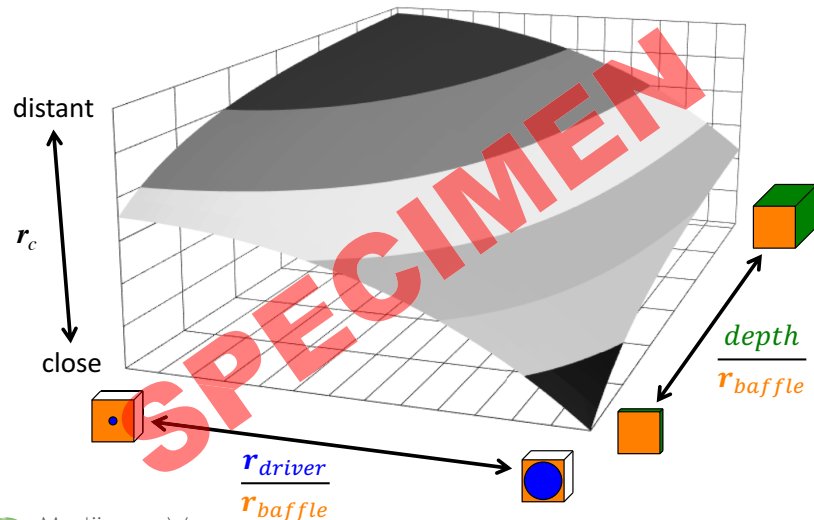


Acoustic Center for LF (Subwoofers)



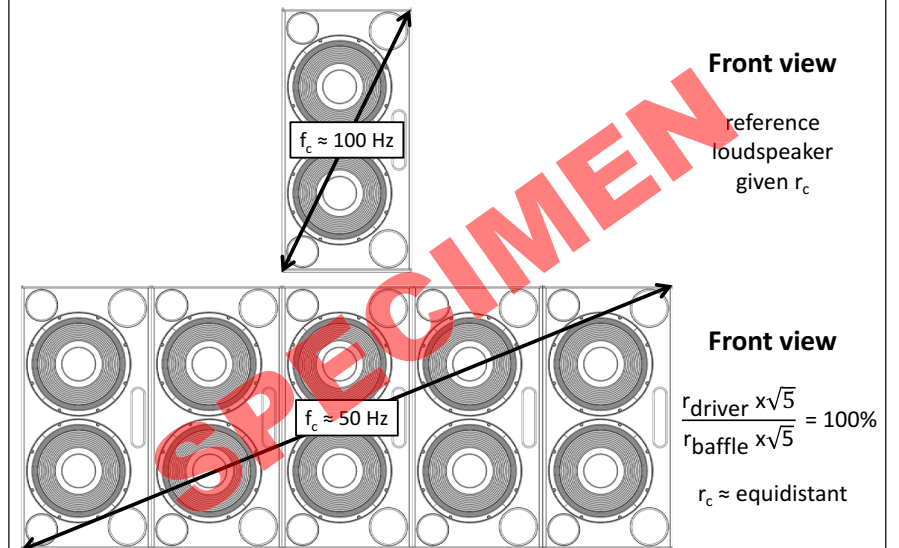
* **DISCLAIMER:** Research limited to sealed and vented enclosures only

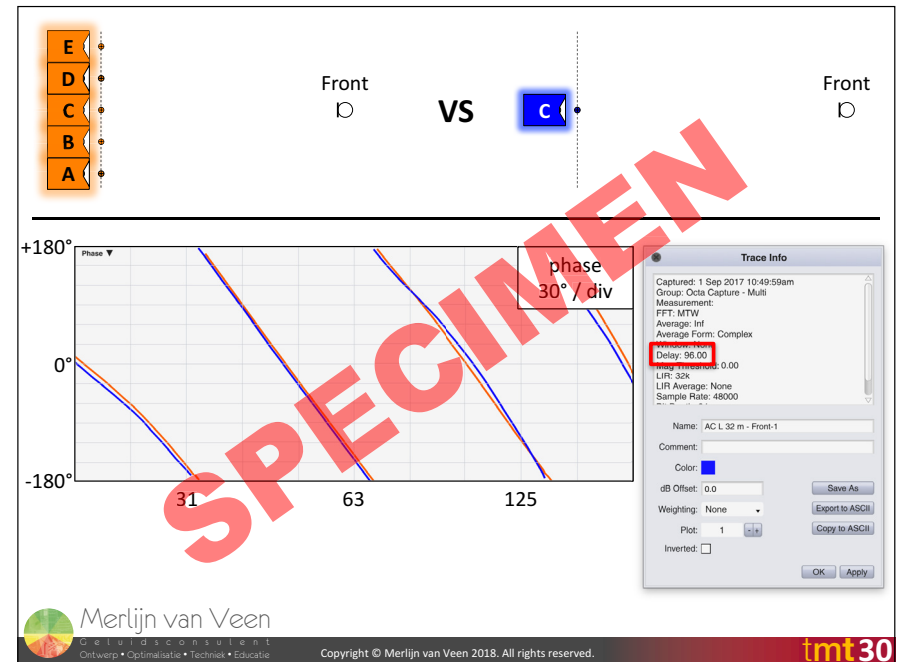
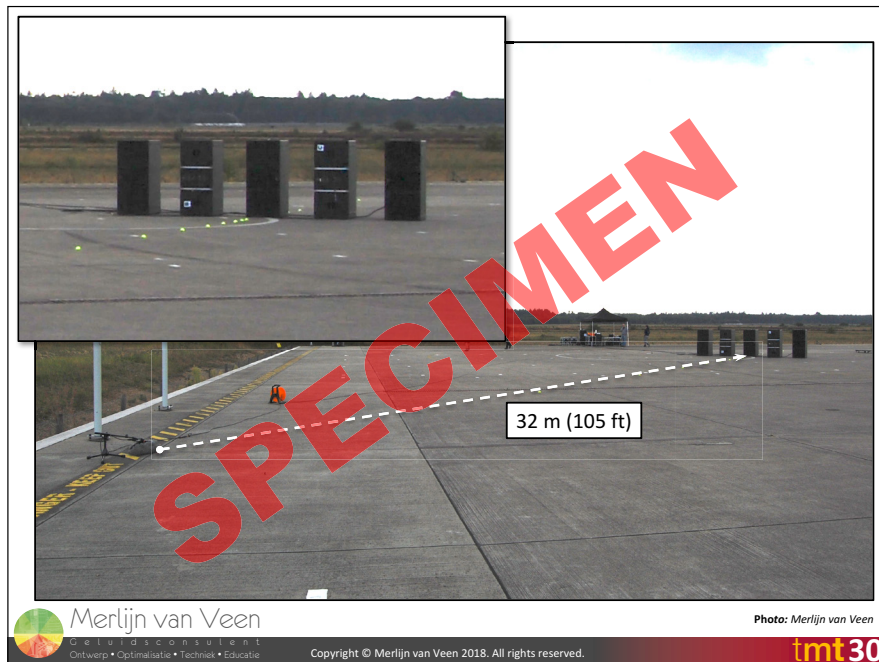
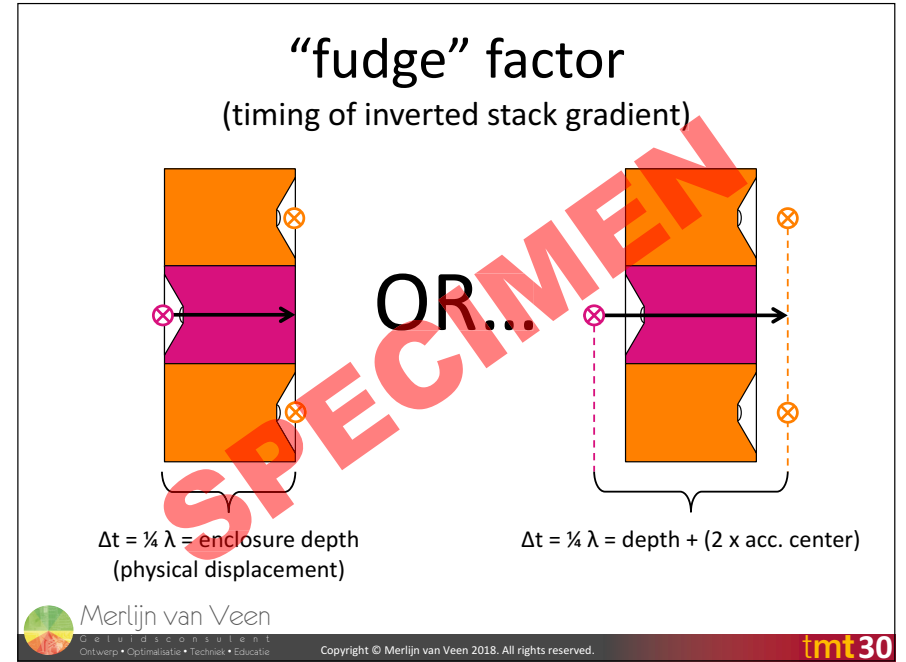
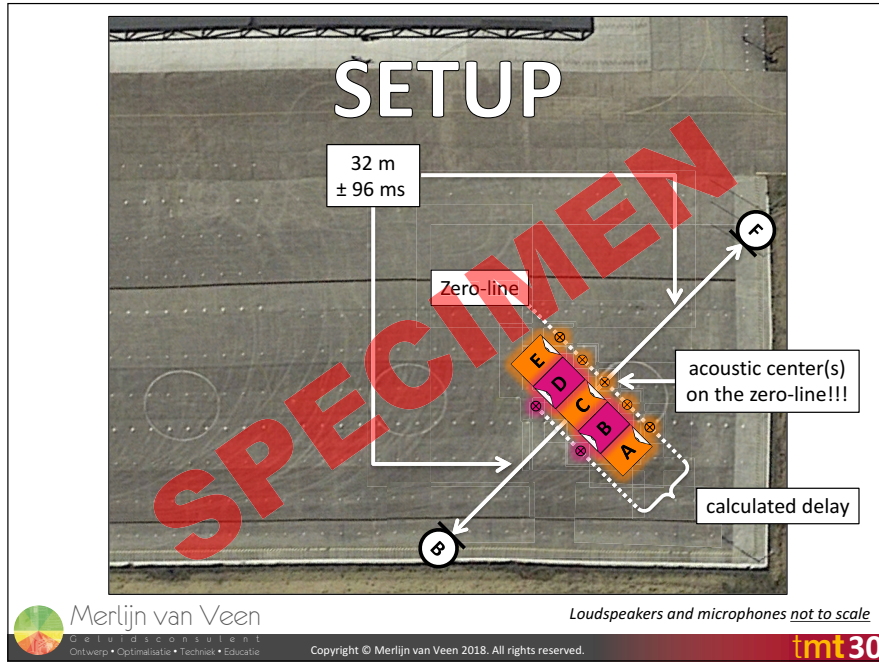
Acoustic Center for LF (Subwoofers)

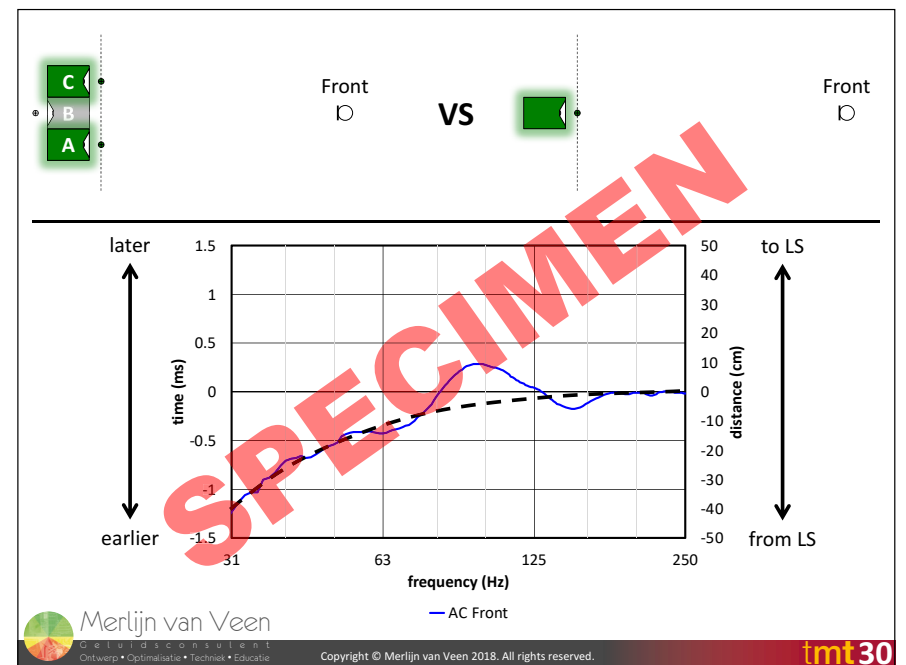
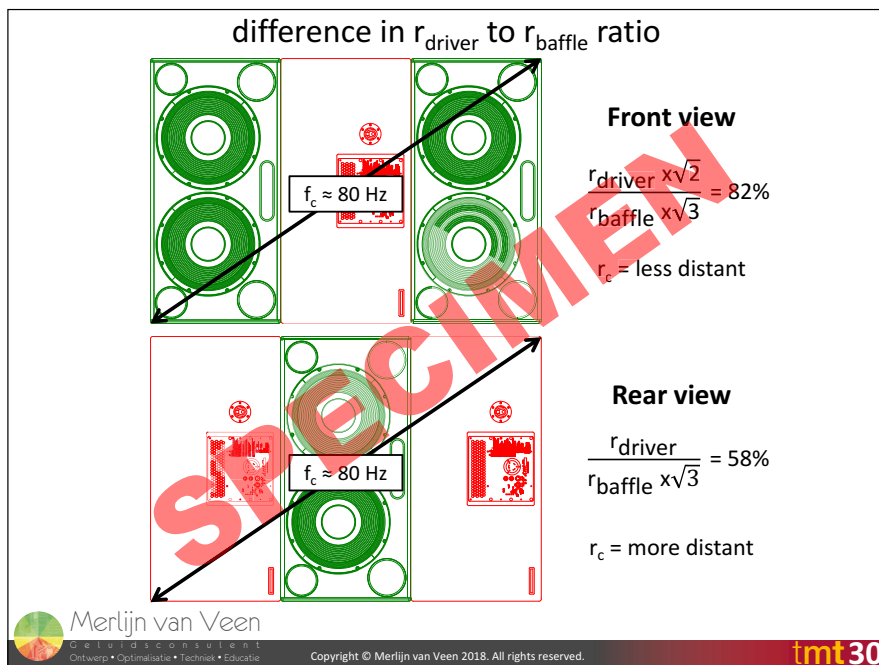
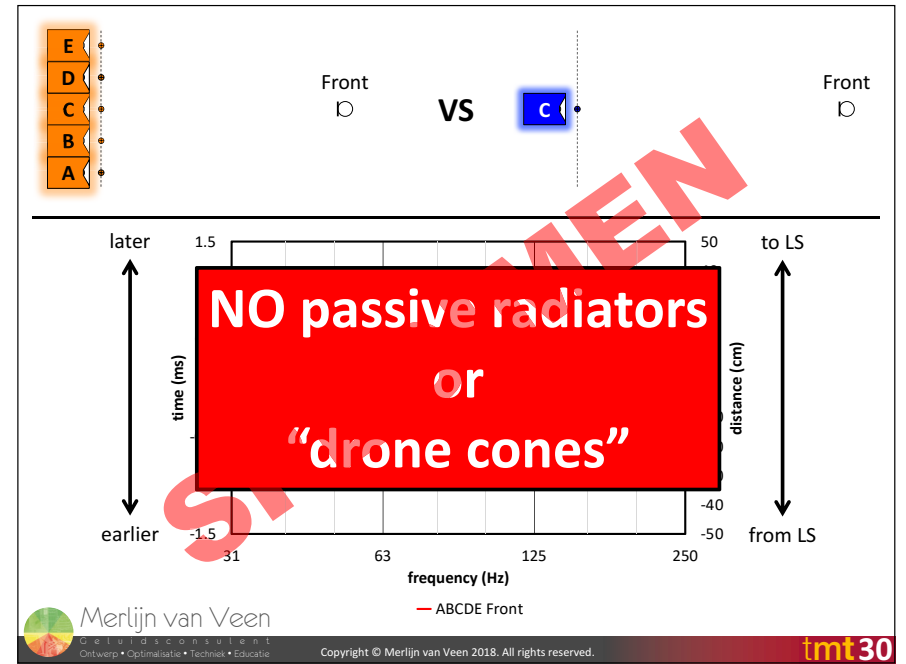
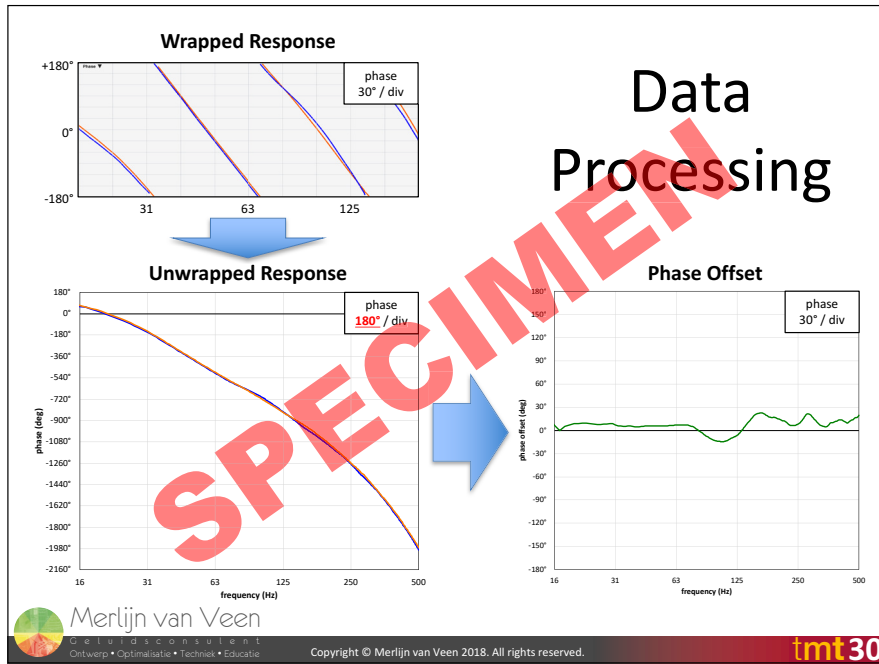


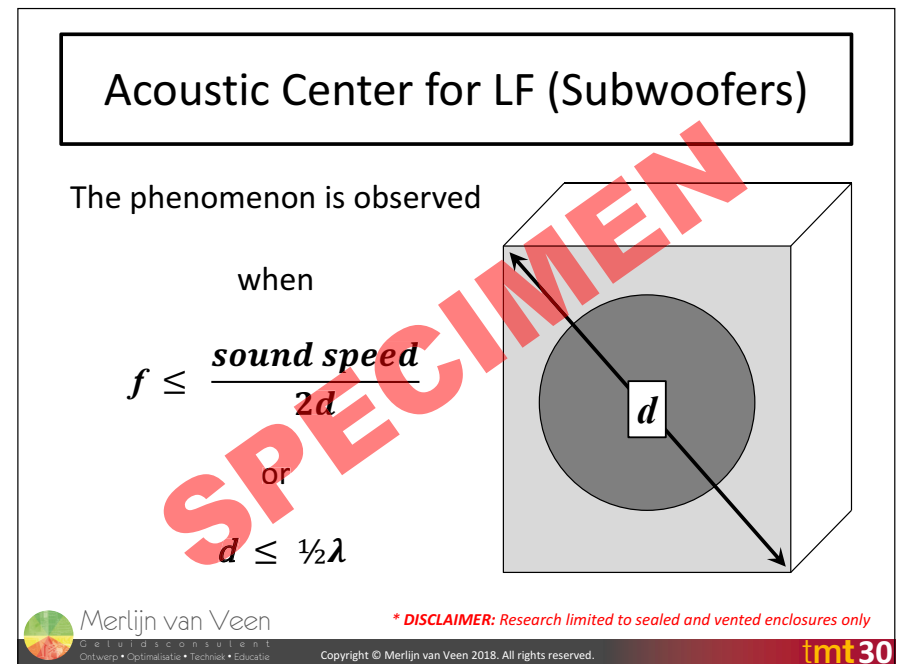
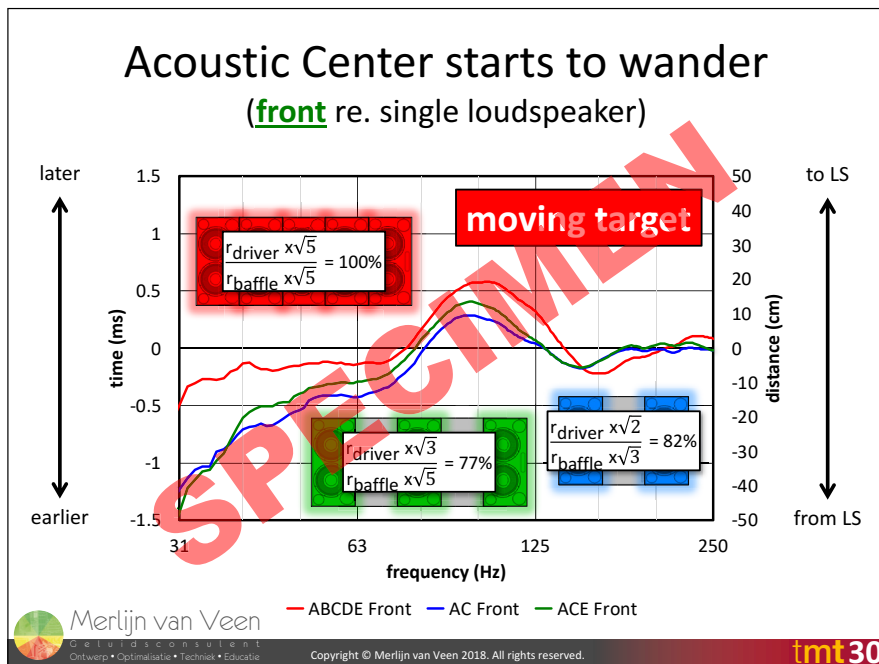
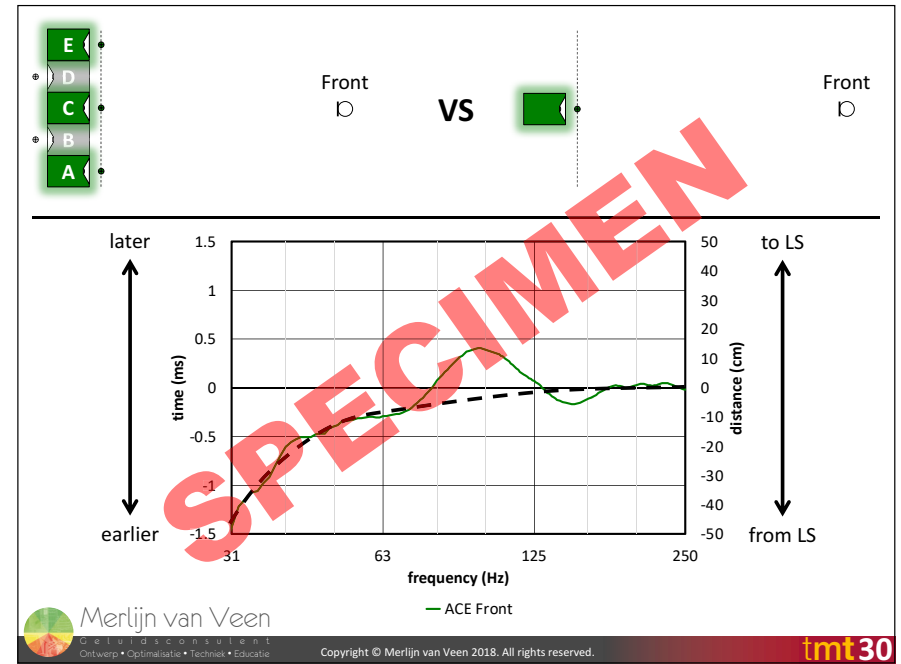
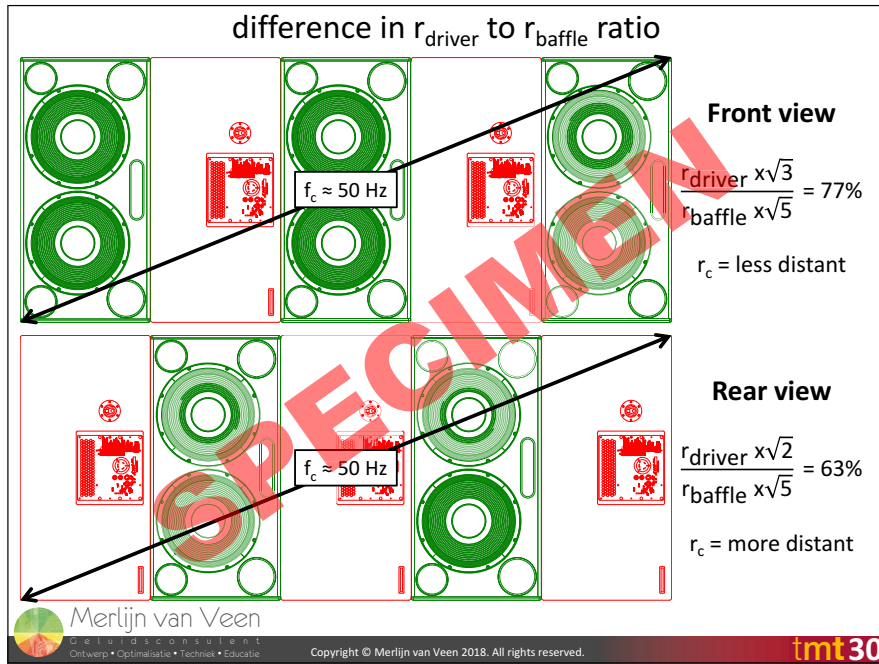
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difference in r_{driver} to r_{baffle} ratio

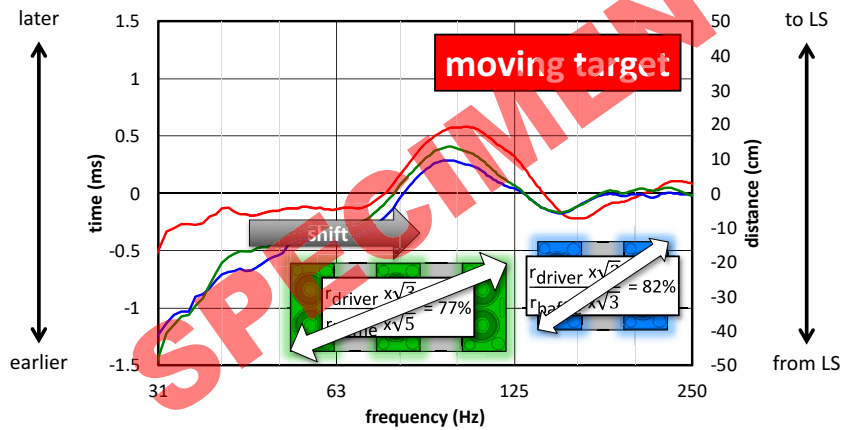




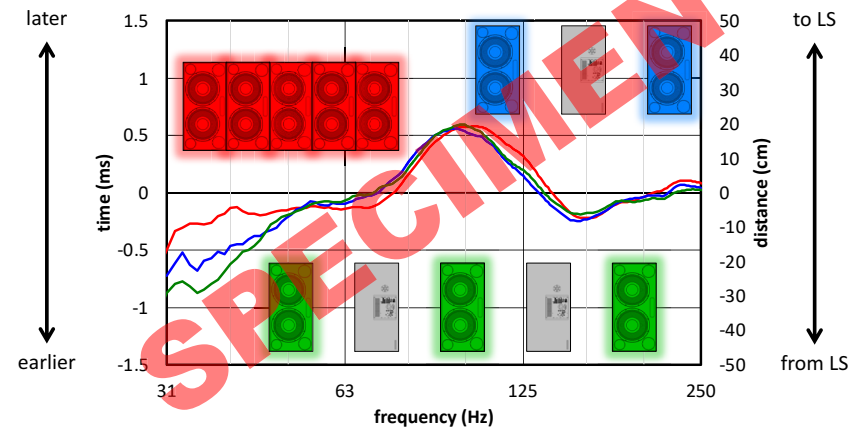




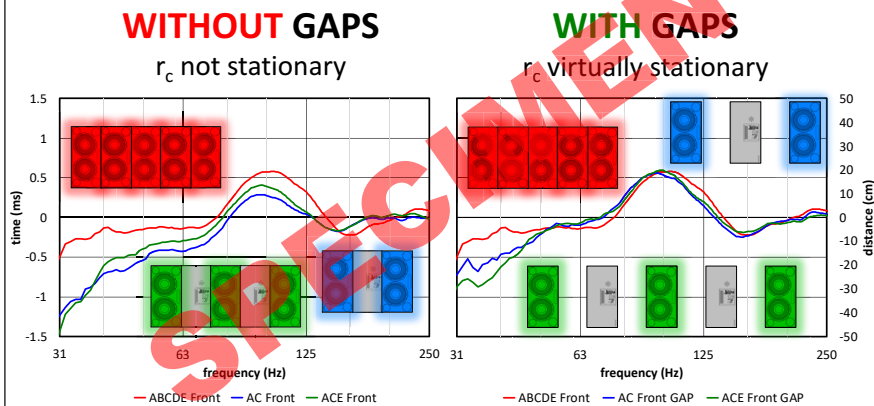
Acoustic Center starts to wander (front re. single loudspeaker)



Acoustic Center starts to wander (front re. single loudspeaker)

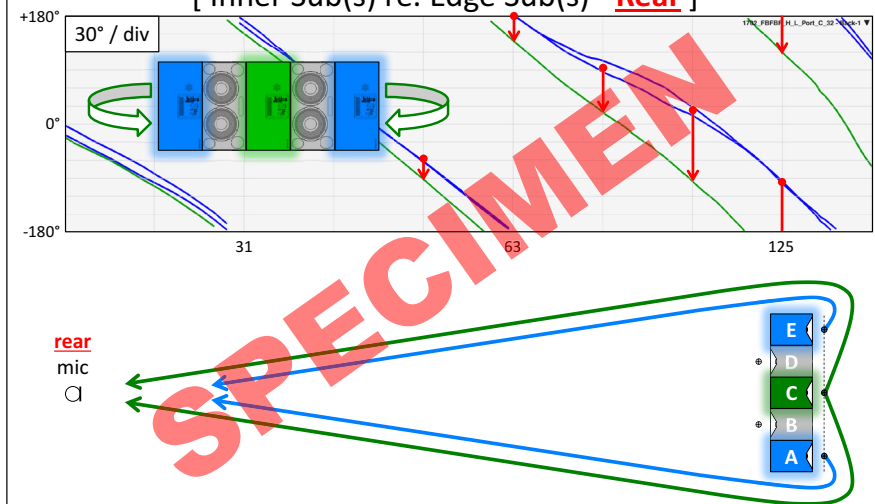


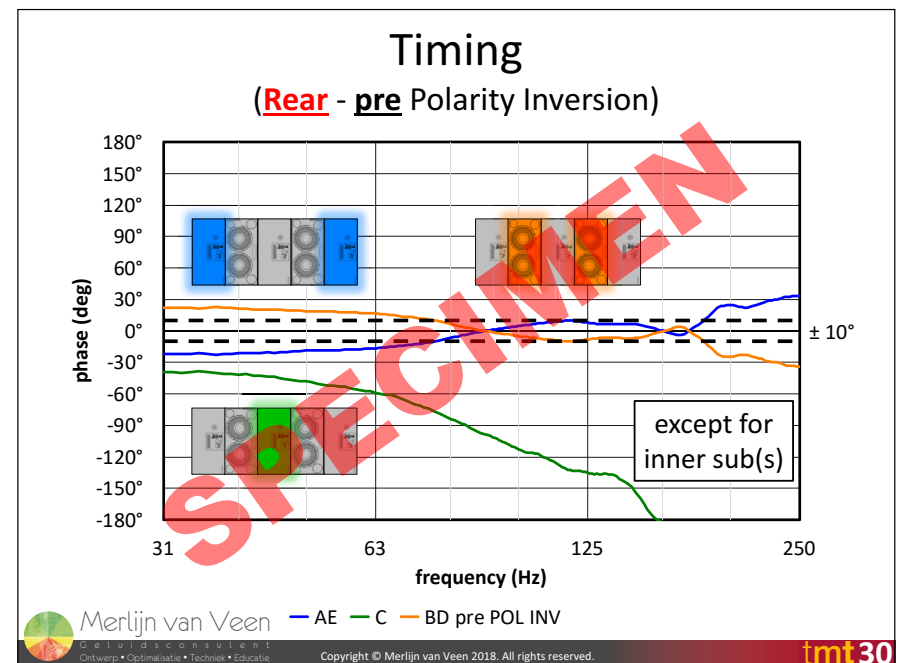
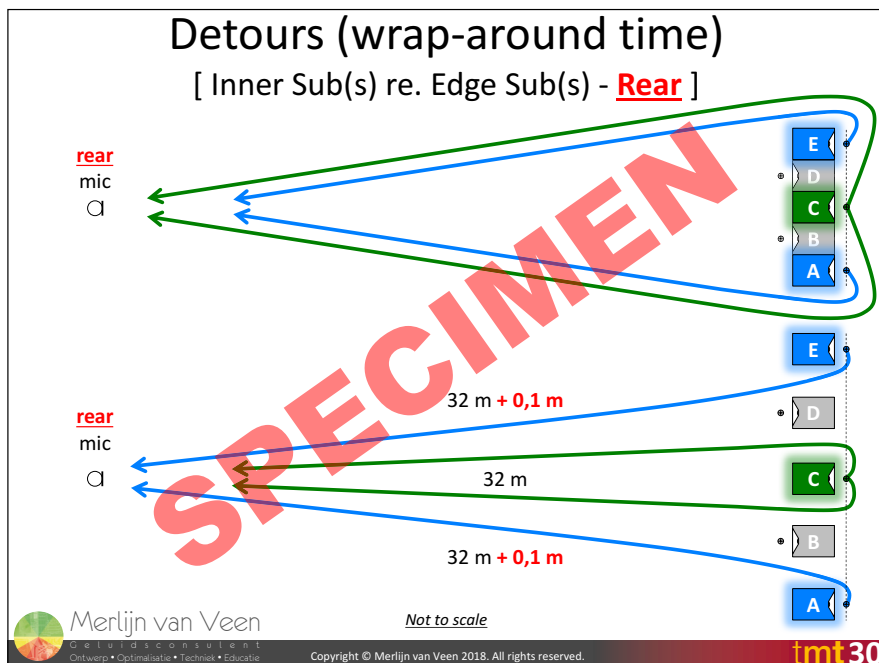
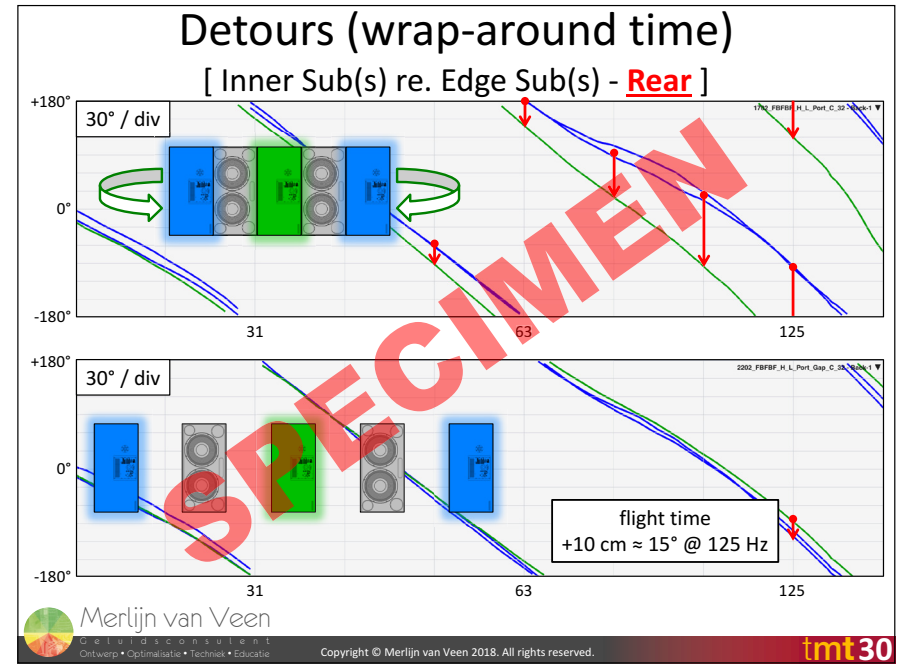
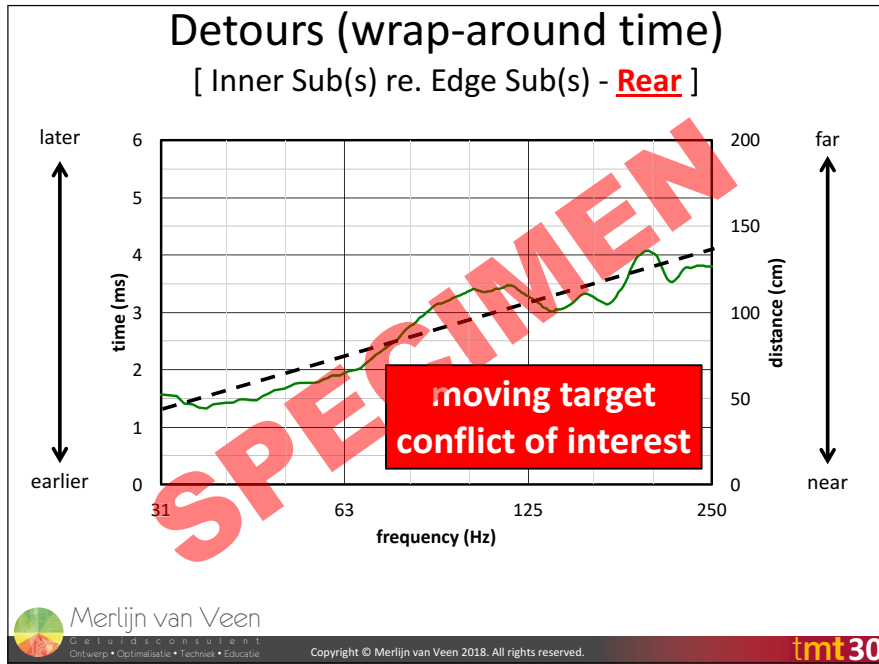
Acoustic Center starts to wander (front re. single loudspeaker)

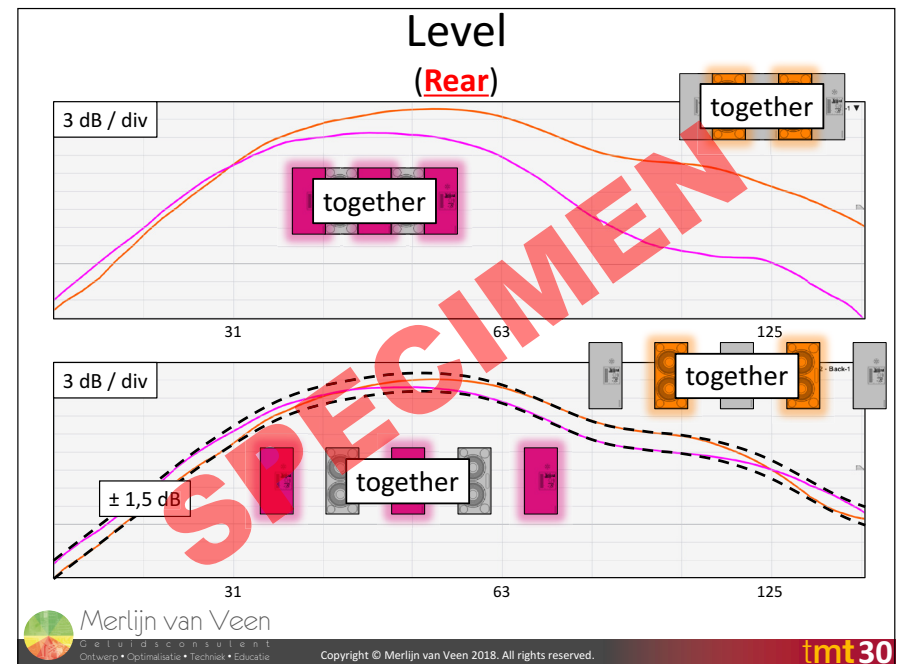
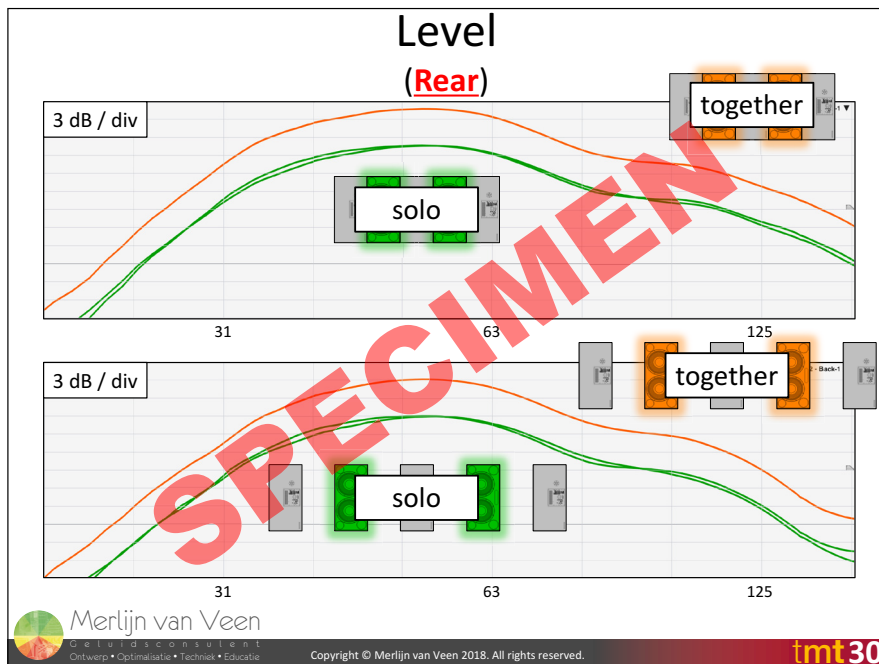
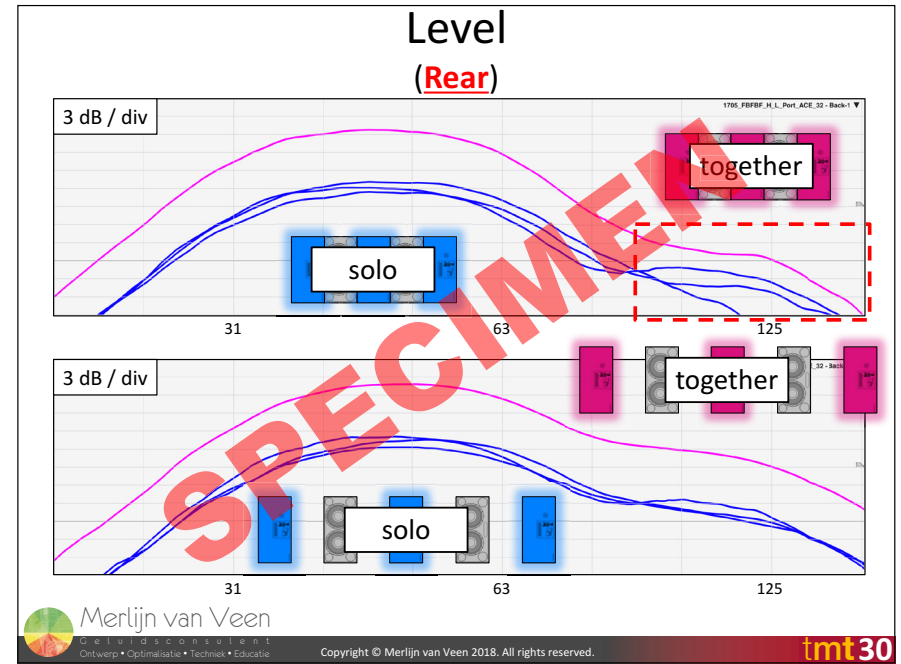
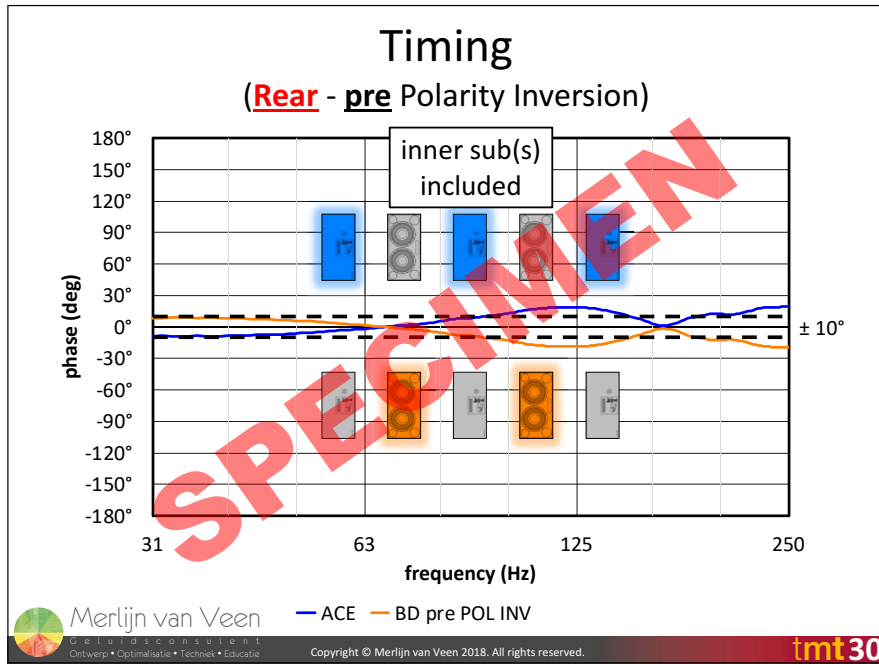


Detours (wrap-around time)

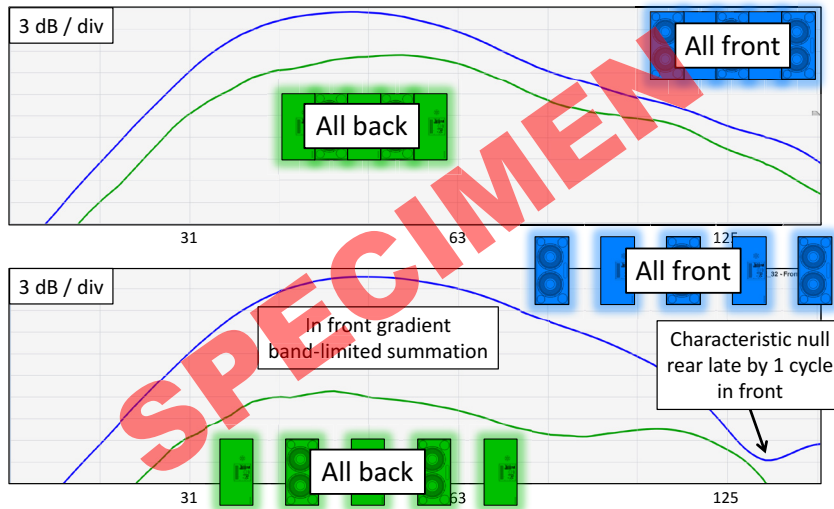
[Inner Sub(s) re. Edge Sub(s) - Rear]







Front-2-Back Difference



Conclusion

Without Gaps

- acoustic center not stationary
 - array configuration dependent
 - frequency dependent
- (physical) detours in opposite direction (wrap-around time)
 - inner sources take longer than edge sources
 - frequency dependent
- level variance due to diffraction
 - frequency dependent
- hard to predict (PSM falls short)
- every array configuration requires custom preset

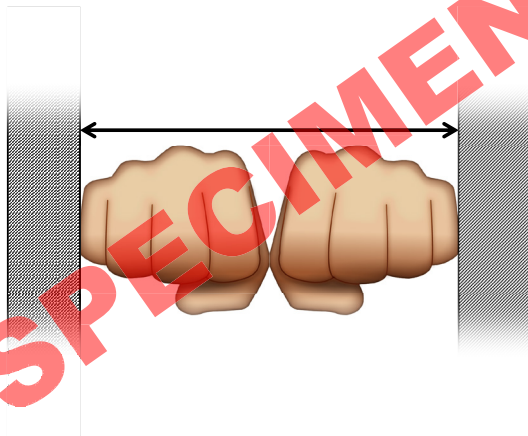
With Gaps

- acoustic center virtually stationary
 - array configuration independent
- no (physical) detours
 - inner- and edge-sources arrive in time*
- matched levels (little to no diffrac.)
 - provided front- and rear-facing sources have the appropriate ratio to complement polar plot
- no pattern implosion
- predictable
- modular & scalable
 - one preset suffices

* Flight time not taken into account

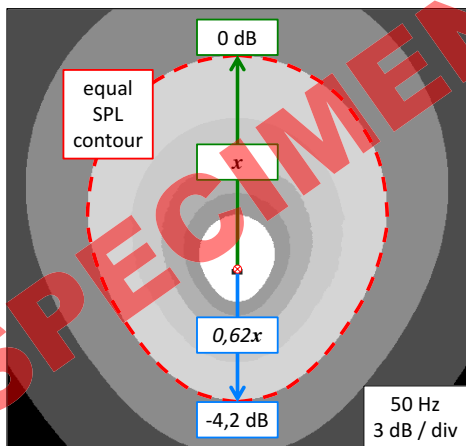
Two Fists

(minimum spacing - experimentally determined)



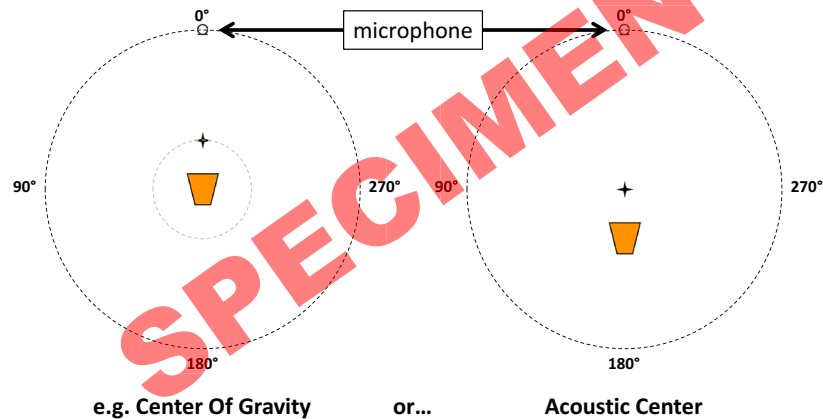
Food for thought...

(Vented enclosure - Dual 18" Direct Radiators)



Polar plots for Subwoofers

(Center of Rotation During Measurement)



Thank you!

Credits

Companies

- Audio Electronics Mattijsen
- Heijmans
- National Military Museum
- Sound & Light Import

People

- Timo Beckman
- Tom de Haas
- Dico ter Maten
- Vince van Seggelen
- Lieven Verzele